







U.S. Army Coast, Eng. Res. Ctr. Tech. Rep. CER AUBITEY

TECHNICAL REPORT CERC-87-9

## BEACH AND NEARSHORE SURVEY DATA: 1981-1984 CERC FIELD RESEARCH FACILITY

by
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July 1987 Final Report

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| SECURITY CLASSIFICATION OF THIS PAGE   |   |   |   |                                     |   |
|--|---|---|---|-------------------------------------|---|
| REPORT D   | OCUMENTATIO   | N PAGE  |   |                                     | Form Approved<br>OMB No. 0704-0188<br>Exp. Date: Jun 30, 1986 |
| 1a. REPORT SECURITY CLASSIFICATION   |   | 1b. RESTRICTIVE   | MARKINGS  |                                     |   |
| Unclassified   |   |   |   |                                     |   |
| 2a. SECURITY CLASSIFICATION AUTHORITY  |   | 3. DISTRIBUTION/AVAILABILITY OF REPORT                      |   |                                     |   |
| 2b. DECLASSIFICATION / DOWNGRADING SCHEDULE  |   | Approved for public release; distribution unlimited         |   |                                     |   |
| 4. PERFORMING ORGANIZATION REPORT NUMBE  | R(S)  | 5 MONITORING  | ORGANIZATION R  | EPORT NIL                           | IMBER(S)  |
| Technical Report CERC-87-9   |   | 5. MONITORING ORGANIZATION REPORT NUMBER(S)                 |   |                                     |   |
| 6a. NAME OF PERFORMING ORGANIZATION USAEWES, Coastal Engineering (If applicable)   |   | 7a. NAME OF MONITORING ORGANIZATION                         |   |                                     |   |
| Research Center  |   |   |   |                                     |   |
| 6c. ADDRESS (City, State, and ZIP Code)  |   | 7b. ADDRESS (Cit  | y, State, and ZIP   | Code)                               |   |
| PO Box 631<br>Vicksburg, MS 39180-0631   |   |   |   |                                     |   |
| 8a. NAME OF FUNDING/SPONSORING<br>ORGANIZATION   | 8b. OFFICE SYMBOL<br>(If applicable)                                      | 9. PROCUREMENT  | I INSTRUMENT ID   | ENTIFICAT                           | TION NUMBER   |
| US Army Corps of Engineers   |   |   |   |                                     |   |
| 8c. ADDRESS (City, State, and ZIP Code)  |   |   | UNDING NUMBER   |                                     | Turoni i ini  |
| Washington, DC 20314-1000  |   | PROGRAM<br>ELEMENT NO.                                      | PROJECT<br>NO.  | TASK<br>NO.                         | ACCESSION NO.   |
| 11. TITLE (Include Security Classification)  |   |   |   |                                     |   |
|  |   |   |   |                                     |   |
| Beach and Nearshore Survey Da  | ta: 1981-1984,  | CERC Field F  | Research Fac  | ility                               |   |
| 12. PERSONAL AUTHOR(S)   |   |   |   |                                     |   |
| Howd, Peter A., Birkemeier, W  |   |   |   |                                     |   |
| Final report FROM FROM   | OVERED TO   | 14. DATE OF REPO<br>July 1987                               | RT (Year, Month,  | Day) 15                             | i. PAGE COUNT<br>143  |
| 16. SUPPLEMENTARY NOTATION<br>Available from National Techn<br>Springfield, VA 22161.  | ical Information  | Service, 52   | 285 Port Roy  | al Roa                              | d,  |
| 17. COSATI CODES   | 18. SUBJECT TERMS (   | Continue on revers  | e if necessary and  | didentify                           | by block number)  |
| FIELD GROUP SUB-GROUP  | Beaches   | Field Res   | earch Facil   | ity                                 |   |
|  | CRAB  | Profile c   |   |                                     |   |
|  | Duck, NC  | Profile d   | ata   |                                     |   |
| 19. ABSTRACT (Continue on reverse if necessary   | and identify by block n   | umber)  |   |                                     |   |
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| The data were collected<br>motorized tripod, which, comb<br>is capable of accuracies of a  | ined with an ele  | ectronic "tot   | tal station'  | surve                               | ying instrument,  |
|  |   |   |   |                                     | (Continued)   |
| 20. DISTRIBUTION / AVAILABILITY OF ABSTRACT  |   | 21. ABSTRACT SE   | CURITY CLASSIFIC  | ATION                               |   |
| UNCLASSIFIED/UNLIMITED SAME AS   | RPT. DTIC USERS   | IInclassi   | fied -  |                                     |   |
| 22a. NAME OF RESPONSIBLE INDIVIDUAL  |   | 22b. TELEPHONE (  | Include Area Code   | ) 22c. O                            | FFICE SYMBOL  |
|  |   |   |   |                                     |   |
|  | PR edition may be used un   |   |   | CLASSIFIC                           | ATION OF THIS PAGE  |



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| 19. | ABSTRACT | (Continued). |  |
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The report discusses the data-collection methods, the sources of errors and data-editing procedures, and a brief summary of the actual profile data. Appendices contain the listings and plots of the survey data along with the tables and plots of the wave and water-level data.

#### PREFACE

This report was prepared at the Coastal Engineering Research Center (CERC) of the US Army Engineer Waterways Experiment Station (WES) as part of the Storm Erosion Studies Work Unit, Shore Protection and Restoration Program; Coastal Engineering Area, Civil Works Research and Development. Technical Monitors were Mr. John H. Lockhart, Jr., and Mr. John G. Housley, Headquarters, US Army Corps of Engineers.

Mr. Peter A. Howd and Mr. William A. Birkemeier of CERC's Field Research Facility Group prepared the report under the supervision of Mr. Curt Mason, former Chief, Field Research Facility; Mr. Thomas W. Richardson, Chief, Engineering Development Division; and Mr. Charles C. Calhoun, Jr., and Dr. James R. Houston, Assistant Chief and Chief, CERC, respectively. Messrs. Eugene W. Bichner, Charles R. Townsend III, Michael W. Leffler, Francis E. Sargent, and Ms. Rebecca J. Savage, plus many others, contributed to the collection of the data. Ms. Harriet M. Klein assisted greatly by untangling complexities of the English language. The wave and water-level data presented in the report were collected by CERC's Field Research Facility Measurements and Analysis Work Unit under the direction of Mr. Herman C. Miller. This report was edited by Ms. Jamie Leach of the WES Information Technology Laboratory.

Commander and Director of WES upon publication of this report was COL Dwayne G. Lee. Technical Director was Dr. Robert W. Whalin.

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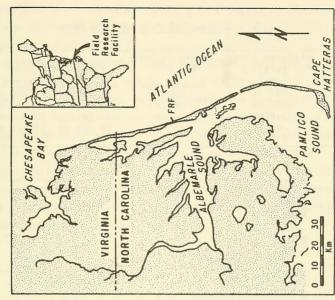
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# BEACH AND NEARSHORE SURVEY DATA: 1981-1984 CERC FIELD RESEARCH FACILITY

#### PART I: INTRODUCTION

- 1. The Field Research Facility (FRF) of the US Army Engineer Waterways Experiment Station (WES), Coastal Engineering Research Center (CERC), was established to provide a research and development capability for field studies of coastal processes. An important part of the FRF operation has been the collection of long-term data sets of waves, currents, tides, atmospheric conditions, and beach profile change. The purpose of this report is to present the first 4 years of highly accurate profile data collected under the Storm Erosion Studies work unit.
- 2. This continuing data set is unique in the field of beach profile studies because of its accuracy, temporal coverage, and concomitant wave, weather, and water-level information. Surveys of four shore-normal profile lines were completed at approximately 2-week intervals. Nowhere else does such a data set exist. It provides a unique opportunity to examine natural profile changes and to test and evaluate models of beach profile response to changing wave, current, and atmospheric conditions.
- 3. The FRF is located just north of the village of Duck, N. C., on the Outer Banks (Figure 1). The facility includes a 561-m-long research pier and support buildings. The beach adjacent to the study area is interrupted only by open pile piers from Cape Henry, Va., to Oregon Inlet, N. C., a distance of 110 km. General information regarding the FRF and the surrounding area is provided in Birkemeier et al. (1985). A comprehensive network of weather and ocean sensors provides continuous monitoring of atmospheric and oceanographic conditions. These data are published in a series of annual (Miller 1984; Miller et al. 1985, 1986) and monthly data reports.
- 4. The data in this report were collected along the four profile lines shown in Figure 2 (Lines 58, 62, 188, and 190). A profile line is defined as a fixed transect across the beach and nearshore which is repetitively surveyed. Table 1 summarizes the location of these lines and the data contained in this report. Based on regular monthly surveys of the bathymetry



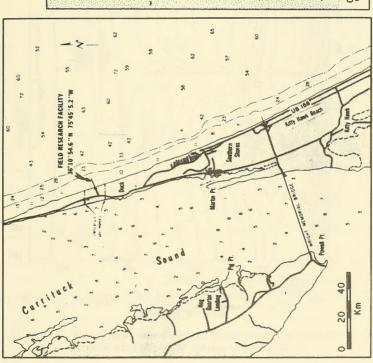


Figure 1. Location of the FRF

Table 1
Summary of Profile Line Data

| Distance Along | Distance From                        |  |   |   |
|----------------|--------------------------------------|--|---|---|
| FRF Baseline   | FRF Pier                             | First  | Last  | Number of   |
| m              | m                                    | Survey   | Survey  | Surveys   |
| 1097.31        | 580.64                               | 17 Jul 81  | 13 Dec 84   | 96  |
| 1005.84        | 489.21                               | 26 Jan 81  | 13 Dec 84   | 119   |
| 0.00           | -516.63                              | 20 Jan 81  | 17 Dec 84   | 127   |
| -91.40         | -608.07                              | 17 Jul 81  | 17 Dec 84   | 99  |
|                | FRF Baseline  m 1097.31 1005.84 0.00 | FRF Baseline FRF Pier  m m  1097.31 580.64  1005.84 489.21  0.00 -516.63 | FRF Baseline         FRF Pier         First           m         m         Survey           1097.31         580.64         17 Jul 81           1005.84         489.21         26 Jan 81           0.00         -516.63         20 Jan 81 | FRF Baseline         FRF Pier         First         Last           m         m         Survey         Survey           1097.31         580.64         17 Jul 81         13 Dec 84           1005.84         489.21         26 Jan 81         13 Dec 84           0.00         -516.63         20 Jan 81         17 Dec 84 |

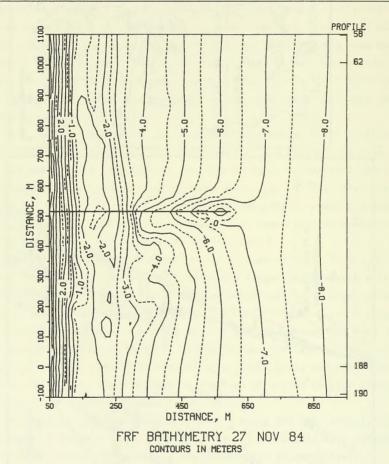


Figure 2. Bathymetric map of the study area showing locations of the four profile lines

surrounding the FRF, these lines are located in a region of shore-parallel contours and are sufficiently removed from known pier effects (Miller, Birkemeier, and DeWall 1983).

- 5. The beach is composed of a mixture of quartz sand and carbonate shell debris. The carbonate component may be as high as 20 percent. Mean grain size is greatest on the foreshore where it approaches 1 mm, decreasing offshore to 0.1 mm. Sorting improves in an offshore direction. Figure 3 illustrates the cross-shore variation in sediment size distribution based on a series of samples taken along profile line 188 on 17 March 1982.
- 6. Storm conditions at the FRF are dominated by extratropical northeasters during the winter months and occasionally by tropical hurricanes. During the period of study, a number of significant storms occurred, although no major hurricanes passed the area.

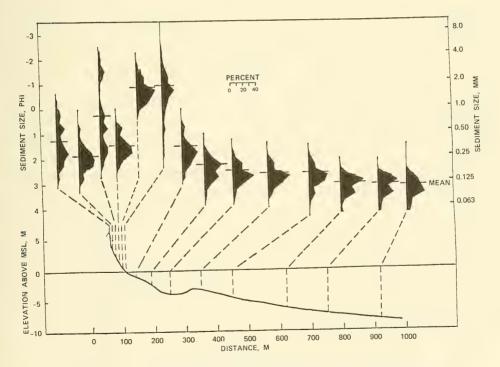


Figure 3. Distribution of sediment sizes across profile line 188 on 17 March 1981

7. The report includes five parts and six appendices. Part II discusses the survey methods used to collect the profile data and points out the sources of errors and methods used to minimize those errors. Part III presents summary comments about profile characteristics and patterns of profile change as an aid in interpreting the data. Part IV presents the associated wave and water-level data. The report is summarized in Part V. Appendices include plots of all the profiles (Appendix A), tables of the profile data along with a FORTRAN computer program to read and check the data (Appendices B and C), plots of wave height for the 4-year period (Appendix D), tables of wave height and period (Appendix E), and plots of the observed tides (Appendix F).

## PART II: PROFILE DATA

- 8. This part describes the methods used to survey the profile data and identifies potential sources of error and how errors were handled. The data for each profile line are a series of distance-elevation pairs measured during a repetitive number of surveys. The data extend from a shore-parallel base-line, located landward of the duneline, out to a usual depth of 8 to 9 m. Elevation data are referenced to the 1929 National Geodetic Vertical Datum (NGVD) using third-order control established at the FRF. Each survey of each profile line is uniquely identified by a profile number and survey number.
- 9. Surveys were initially conducted biweekly, the northern lines one week followed by the southern lines the next. This sequence changed in December 1982 to biweekly surveys of all four lines. Full bathymetric surveys of 15 to 28 lines surrounding the FRF were also conducted monthly. Additional surveys were added to cover significant storms and in support of special experiments. The time interval between surveys varied from 1 to 44 days.

## The CRAB

- 10. The method used to collect the majority of the profile data is described in Birkemeier and Mason (1984). All profiles were surveyed using the FRF Coastal Research Amphibious Buggy (CRAB) shown in Figure 4. Built by the Wilmington District of the US Army Corps of Engineers, this unique three-wheeled vehicle was modeled after a vehicle originally built by Marine Travelift & Engineering of Sturgeon Bay to monitor a Corps of Engineers beach nourishment project.
- 11. The CRAB consists of a tripod of 20.3-cm schedule-80 aluminum tubing, connected at the base by horizontal members 2.1 m above the ground, and an operations platform 10.7 m above the ground. Power is supplied by a 39.5-kW Volkswagen engine on the deck which drives a variable stroke hydraulic pump. This pump transfers hydraulic fluid at  $5.5 \times 10^6 \ \mathrm{N/m^2}$  or higher to hydraulic motors at each of the wheels. The variable stroke feature of the pump allows an infinitely variable gear ratio in either forward or reverse and constant engine speed. For strength and corrosion resistance, all hydraulic lines are stainless steel except for short flexible sections at the front steering wheel.



Figure 4. The CRAB

- 12. Total vehicle weight is about 8,200 kg; the distance between the rear wheels is 8.2 m. Though it appears top heavy, the liquid-filled tires and wide wheelbase make it very stable. It has passed a 20-deg tilt test and is designed to withstand even steeper angles.
- 13. Top speed of the CRAB is 3.2 km/hr on land and somewhat less in the water. Since the maximum significant wave height for operation is 2 m, the CRAB is capable of operating in all but the most severe east coast storms. The large tires have a negligible effect on a hard rippled sand bottom; however, scour around the tires has been observed in areas of active wave breaking or strong currents if the CRAB remains motionless. The CRAB cannot be used on soft silty or loose bottoms.
  - 14. All beach and dune surveying was accomplished with the standard

technique of sending a rodperson along the transect, stopping at regular intervals and breaks in slope.

## Early Stadia Surveys

- 15. From January to June 1981, the position and elevation of the CRAB were determined using an automatic level, located on the beach, to read a 12.3-m-high stadia board attached to the CRAB. This system was slow and sensitive to a wide range of errors. Primary sources of error included out-of-level or poorly aligned instruments, stadia reading errors, fieldbook and transcription errors, and instrument stationing errors. Estimated accuracy in distance was from ±0.3 to ±6 m. Vertical accuracy was estimated to vary from ±0.03 to +0.6 m. Single points or surveys may have been in greater error.
- 16. Errors tended to increase with distance. This resulted from the increased difficulty in reading the stadia board and the greater impact of out-of-level errors. Because of these errors, data collected prior to June 1981 end approximately 600 m offshore. Points farther offshore were of questionable accuracy and have been dropped.
- 17. Although of inferior quality to later surveys, the stadia survey data have been retained in the data set because the configuration of the profile lines (which is accurately represented) during this period is unusual and not later repeated.

## Electronic Survey System

18. In order to improve the speed and accuracy of the surveys, a Zeiss Elta-2 electronic surveying instrument with automatic data recording was used after June 1981 (Figure 5). This instrument incorporates in one compact unit a first-order electronic theodolite, distance meter, microprocessor, rechargeable power supply, and interchangeable solid state memory module. When optically aimed at a reflecting prism on the CRAB, the instrument uses a collimated infrared beam to measure the distance and the electronic theodolite to measure both horizontal and vertical angles. The microprocessor then uses these measurements plus the coordinates of the instrument to compute X, Y, and Z Cartesian coordinates of the ground point under the CRAB (corrected for



Figure 5. Zeiss Elta-2 electronic surveying instrument

earth curvature).

- 19. The stated operating range is 2 km with a triple prism assembly as used on the CRAB. Working accuracy of  $\pm 3$  cm or better is possible in both horizontal and vertical coordinates. Actual accuracy in a repetitive survey program is less because of changing atmospheric conditions, different instrument setups, and differences in the actual points surveyed.
- 20. The high accuracy of the system is shown in Figure 6 (Birkemeier and Mason 1984), which shows 10 repetitive surveys of a profile line collected over a 2-day period under near ideal conditions. While there is movement of the nearshore bar during the period shown, the stability of the offshore zone is of greater interest. Seaward of 220 m, the average range in elevation was 5 cm. The standard deviation of the 10 elevations for a given distance was usually less than 2 cm.
- 21. Only about 10 sec are required to aim, shoot, and record each survey point. Because the actual coordinates of each point are displayed, the CRAB can easily be kept on line to within  $\pm 1.5$  m through radio communications between the CRAB driver and the instrument operator.

- 22. Once the survey is complete, the solid state memory is removed from the Zeiss, and the data are transferred through a Zeiss interface to a main-frame, desktop, or minicomputer. Because the system only requires proper aim from the operator, instrument reading errors and fieldbook entry errors are eliminated.
- 23. A unique feature of the Zeiss system is its ability to accept and record an additional piece of information (up to seven digits) with every survey point. This was used to manually enter the angular tilt of the CRAB, which was measured with two orthogonal tilt meters. Up to 14 deg of tilt was recorded on steep portions of the beach. The survey data were adjusted during processing to account for the tilt.

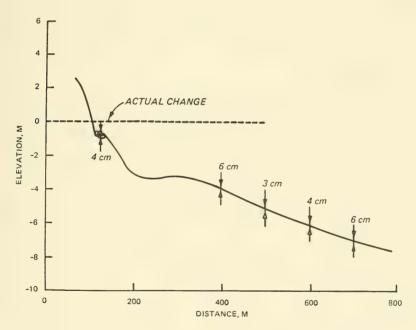


Figure 6. Results of 10 repetitive surveys of a single profile line using the CRAB/Zeiss system

## Error Minimization in Profile Data-Collection Methods

## Error types

- 24. The biases and errors of the CRAB-Zeiss method can be broken down into two distinct categories: limitations of the instrument and operator errors.
- 25. The Zeiss Elta-2 is capable of measuring both horizontal and vertical angles to  $\pm 0.6$  sec of arc and distances to  $\pm 1$  cm in the mode most commonly used at the FRF. The specified range when using a triple prism configuration is 2 km. Increasing the number of prisms increases the range.
- 26. The instrument is sensitive to atmospheric and climatic variation since it uses the speed of light to determine distance and optical aiming to measure the angles. The instrument does allow for rough adjustment for these variables. During the summer months, heat shimmer and temperature gradients near the land-sea interface may also affect the accuracy of the angular measurements. These errors are assumed to be negligible relative to other types of errors.
- 27. On one occasion the Elta-2 developed an internal problem which introduced a gradual bias into the data. This bias was identified and removed during processing. Errors of this type are difficult to remove because they occur radially from the instrument's position and do not uniformly affect the data. The instrument was repaired, and the malfunction did not reoccur. Treatment of errors in the data is discussed below.
- 28. Operator errors can result from improper leveling of the instrument, an error in positioning the instrument in coordinate space (particularly in elevation), movement of the tripod during the survey, and mis-aiming the instrument at the proper location on the prism cluster while taking the measurement. Constructed examples of typical nearshore survey errors and their impact are shown in Figure 7. All the measured points are affected by improper leveling or improper location in coordinate space. Individual points are affected by incorrect aim.
- 29. A different type of operator error results when topographically important points, such as the bar crest or trough, are missed. Survey points are selected based on the timed travel of the CRAB. More points are taken close to shore where the profile is more complex. It is possible for the

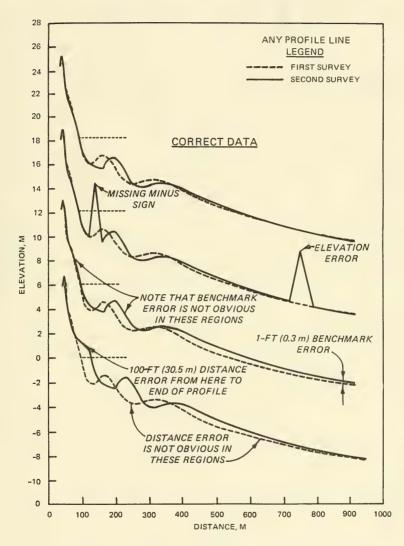


Figure 7. Samples of typical surveying errors and their effects

Zeiss operator to follow the vertical movement of the CRAB, but some significant features were probably missed.

- 30. A third type of operator error is caused by the instrument being triggered to begin a reading prior to properly aiming at the prisms. This short cut of triggering, then sighting the point, results in sampling the azimuth and zenith angles at the time of triggering and later use of these incorrect angles with the distance to the prisms to calculate the CRAB location. Errors affecting single points are usually easy to detect and remove.
- 31. An additional but unquantified source of error results from the thermal expansion and contraction of the CRAB frame and its liquid-filled tires. There is also some "error" introduced into the data by averaging the elevation over the 8.2-m base of the CRAB. The prism and the stadia board were mounted in the vertical plane of the back wheels equidistant between them. Some small error also occurs when sediment is compressed by the weight of the CRAB. Divers have observed tread marks on the bottom following the passage of the CRAB. No adjustment to the data has been made to account for these effects. It is suspected that they may be on the order of 3 to 6 cm. This amount of variation combined with the slight uncertainty of the over 100 different instrument setups results in a survey noise level that obscures small bed-level changes along the offshore reaches of the profiles.

## Error minimization

32. Two steps were taken to minimize the errors associated with the operation of the Zeiss. First, only known locations were chosen as sites for the setup of the instrument, random locations were not used, and each survey always began with a shot to a prism in a known location. If the measured location of the prism was outside certain tolerances, +6 cm horizontal or +1.5 cm vertical, the instrument was restationed. Second, periodic checks to the reference prism during the course of the survey helped ensure that the instrument had neither gone out of level nor was in need of restationing.

## Error identification

33. Errors in the data are most easily recognized through comparison with the past data collected for that profile. All data were compared with the immediately prior survey of the profile. More often than not, this comparison shows where possible errors occur. The suspect points can then be inspected more carefully and a decision made as to whether the point or points were in error or represented real changes on the profile. Figure 7 shows the

utility of comparison. Questionable data, where no clear error could be discerned, were noted and compared with the next survey as well. This provides a double check. Errors were also identified using the measured location of the reference prism shot in during the stationing procedures. Use of these measurements will be discussed in the next section.

## Error correction

- 34. Corrections made to the data consist of two primary types; deletion of points, and addition or subtraction of biases. The biases were either constant because of improper stationing of the instrument or gradual (distance dependent) resulting from improper leveling of the instrument. Vertical errors from mis-leveling become increasingly evident with increasing distance. Vertical corrections to the data were made employing the known elevation of the reference prism and by comparison with surveys of the same profile immediately before and after the questionable data.
- 35. Most often the constant vertical offsets were the result of either improper stationing of the instrument (setting its elevation incorrectly), or, rarely, improper entry of the elevation of the prism cluster on the CRAB. Both of these errors could be traced to the data through the recorded setup procedure. If there was no evidence of a mistake in stationing the Zeiss or entry of the prism height, removal of the suspected bias was dependent on two factors; the bias had to extend over the entire profile (past the normal closure point), and there had to be no reason to expect evidence of profile activity at depth. For instance, if the measured profile showed significant erosion at a depth below the extreme profile closure depth during a period of below-normal wave activity, errors were strongly suspected. However, the bias was removed from the data only after a second survey of the profile further indicated that an error had been made.
- 36. Gradual biases, or rotations of the data, which result from calibration or leveling errors rather than stationing errors, can be more difficult to discern in the data. These corrections were made only to the early level and stadia board data. The shift in the data could be directly attributed to a miscalibration of the automatic level, or to a leveling error during or after setup of the instrument. The rotation needed to correct the data was determined by recalibration of the level.
- 37. Another category of data editing was the removal and/or correction of obviously erroneous data points. These points were usually the result of

improper entry of the height of the CRAB prism cluster into the Zeiss, errors due to the incorrect targeting of the prism cluster, or points which were unaccountably, but obviously, wrong.

- 38. The data were also corrected for the angle of tilt of the CRAB. The CRAB operator measures the two orthogonal angles on the main axes of the CRAB. Angles greater than 4 deg are radioed to the Zeiss operator who enters them into the recorded data. The angles are automatically accounted for during processing of the data.
- 39. Corrections made to the data, (except CRAB tilt corrections), are recorded in processing and data-collection logbooks and are coded into the data file. The meaning and format of the codes are presented in Appendix B.

## Special Notes on the Survey Data

- 40. A number of surveys within the data set require specific discussion regarding data quality. The early stadia surveys (January to 1 June 1981) have already been described. From approximately 14 December 1982 until 9 February 1983, the Zeiss Elta-2 was intermittently producing questionable results which appeared as a systematic vertical error. From 24 February 1983 through 28 March 1983, the instrument was being repaired and alternate methods were employed. These included the use of the stadia board and automatic level to determine elevation and a Motorola Mini-Ranger positioning system to determine offshore distance (24 February to 3 March). A loaner Zeiss instrument was also employed (22 March to 28 March).
- 41. Because this was an unusually active period of profile response with a number of significant storms occurring, the data during this period have been retained in the data set. They do accurately reflect the changes in profile configuration which occurred, but the horizontal and vertical accuracies are less than for the remaining CRAB/Zeiss data.
- 42. Data prior to December 1981 were saved only to whole feet in distance and tenths-of-a-foot in elevation (normal accuracy for beach profile data). Because of the greater accuracy of the CRAB/Zeiss data, subsequent data are stored to tenths-of-a-foot in distance and hundredths-of-a-foot in elevation. This too has an impact on the overall accuracy of the data.

#### PART III: PROFILE RESULTS

- 43. The data presented in this report have been described by Birkemeier (1985a). Some of the discussion from that report is repeated here as an aid in interpreting the data. Profile changes at the FRF occur at time scales ranging from minutes to annual cycles and longer. Time scales resolvable with the data in this report vary between a few days and 1 to 2 years. Though the profiles have varied in configuration from nearly unbarred to triple barred, they typically exhibit a double bar with a narrow and well-defined inner bar and a broad outer bar. Figure 8 illustrates five of the configurations observed during the study.
- 44. The profile envelope defined by all surveys of line 188 is shown in Figure 9. The plot of maximum vertical change in the upper half of Figure 9 indicates most profile activity is restricted to depths less than 7 m with little measurable vertical variation at deeper depths (only 15-cm maximum variation at 8-m depth). It is not clear how much of this 15 cm is real. Birkemeier (1985b) examined the changes within the data set caused by storms and found that significant storm-induced bed-level changes (>3 cm) occurred at depths less than -6.4 m relative to mean low water (-6.8 m below National Geodetic Vertical Datum, NGVD).
- 45. One of the best indicators of profile configuration and activity is the location of the bar crest. Large changes to the profile in terms of volume changes always result in movement of the bar system. Minor storms typically force only the inner bar offshore, while larger storms may move both bars offshore, depositing sand in deeper water. Storm changes were rapid, occurring over periods of 1 to 5 days. The rapidity of these changes is discussed further in Sallenger, Holman, and Birkemeier (1985).
- 46. Onshore bar movement usually corresponded to periods of low waves between storms. The speed and the amount of recovery were affected by the wave conditions and by the poststorm configuration of the profiles. All the bar features tended to disappear during extended periods of low wave conditions.
- 47. An example of the modifications caused by storms is shown in Figure 10. The surveys bracket a series of three storms with the most severe occurring 13-15 November 1981. In contrast, the slow recovery from the changes caused by the fall 1981 storms occurred during 6 months of relatively

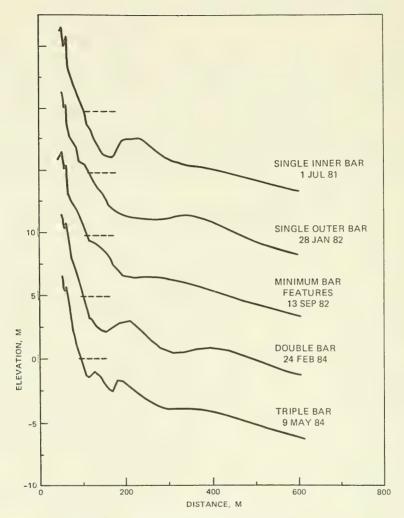
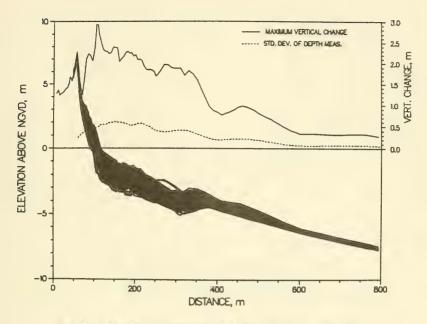


Figure 8. Typical profile configurations occuring in the data set for profile line 62

calm conditions from February to August 1982 (Figure 11).

48. A critical feature of this data set is the fact that four profiles separated in space were measured. Thus, some feeling for the three-dimensional response of the beach is possible. Users of these data are



## PROFILE LINE 188, 127 SURVEYS FROM 20 JAN 81 TO 17 DEC 84

Figure 9. Envelope of all surveys of profile line 188

referred to Sallenger, Holman, and Birkemeier (1985) and Howd and Birkemeier (1987) for a discussion of the rapid three-dimensional changes that have been observed at the FRF. As an example, Figure 12 shows profiles 58 and 62 for a sequence of days during October 1982. Initially, both profiles show the bar moving offshore. By the 15th, the bar has begun to migrate onshore at line 62, but continues to move offshore along line 58. (These two profile lines are separated by less than 100 m.)

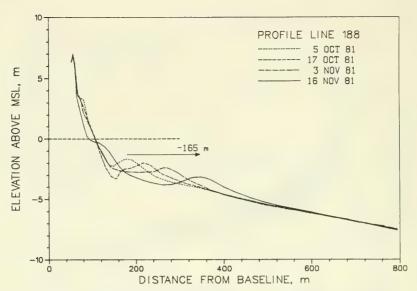


Figure 10. Rapid offshore movement of sediment at line 188 resulting from passage of three fall 1981 storms

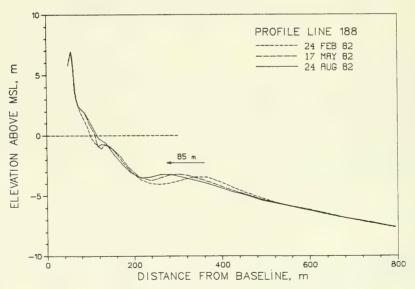


Figure 11. Slow onshore recovery of the outer bar during a 6-month period of low wave conditions

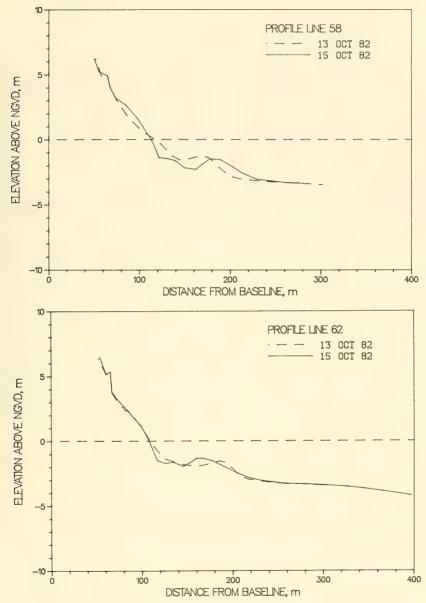


Figure 12. Evidence of three-dimensional profile response at lines 58 and 62 during October 1982

#### PART IV: WAVE AND WATER-LEVEL DATA

## Wave Height and Period

- 49. The wave heights plotted in Appendix D and tabularized in Appendix E were collected as part of the routine collection program of the FRF Measurements and Analysis work unit. Details of the collection of this data are available in the FRF Annual Data Summaries (Miller 1984; Miller et al. 1985, 1986). The data from a number of gages are sampled at 4 Hz, every 6 hr (hourly during storms) for 20 min. The energy-based significant wave height  $H_{m0}$  is computed as four times the standard deviation of the 20-min record. The wave period is computed as period associated with the peak of the wave spectra.
- 50. To provide as complete a record as possible, data from two gages have been combined. The majority of the record is from Gage 625, a Baylor wave staff gage located at the seaward end of the pier. When this gage was inoperative, data from Gage 620, a Waverider buoy located directly off the pier end in 18 m of water, were transformed to the pier end location using the the method of Hallermeier (1983). This method considers frictional dissipation and was developed using data from the FRF.
- 51. During large storms, Gage 625 was in the surf zone and wave heights were saturated, i.e., limited by wave breaking. The maximum wave height limit depends on water level but is usually under 3 m. The maximum recorded wave height of 3.5 m occurred during a storm in November 1981 that coincided with abnormally high spring tides.
- 52. The tables in Appendix E contain daily measurements of wave height and period for wave heights under  $2\ m$  and measurements every  $6\ hr$  for waves over  $2\ m$ .
- 53. More detailed wave information, including wave spectra and data from other gages, is available through the CERC Coastal Engineering Information and Analysis Center (CEIAC).

## Water-Level Data

- 54. The water-level data presented in Appendix F were measured at a National Oceanic and Atmospheric Administration/National Ocean Service (NOAA/NOS) tide station located at the end of the research pier. The data are recorded every 6 min. NOS interpolates missing values using data from nearby gages, accounting for known time lags and elevation differences. The data presented in Appendix F represent the total water-level variation including both the astronomical tides and storm surges. The storm surge is usually defined as the difference between the actual water level and the predicted tides. The total water level should give a better indication of possible forcing of profile change than would the predicted tides or storm surge alone.
- 55. Because of the voluminous amount of water-level data, Appendix F includes only plots of the water level. More detailed data are available through CEIAC or from NOAA/NOS.

## PART V: SUMMARY

- 56. Four years of high-quality beach profile data collected at the FRF are presented. These data are unique in that they cover the most active part of the profile from the dune out past the depth of closure. The data offer a rare look at the dynamic and often surprising changes that naturally occur in the nearshore zone. The majority of the profile data were collected using the FRF CRAB and a highly accurate electronic surveying instrument. Some relevant dynamic parameters to profile change (wave height, period, and observed tides) are also presented.
- 57. The data should be useful to coastal engineers and researchers who need to have an understanding of the dynamic nature of the nearshore zone. They can provide input and calibration data to numerical and physical models of profile changes. Long-term and seasonal profile envelopes can be computed and used as a guide for determining cable and ocean outfall burial depths and where best to place wave- and current-measuring instruments.

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## APPENDIX A: SURVEY PLOTS, 1981-1984

This appendix contains plots of the survey data included in Appendix B. The plots are presented by profile number, starting from the north end of the Field Research Facility property. Refer to Figure 1 of the main text for the location of the profile lines with respect to the pier. Each profile is plotted along with the preceding profile; thus, the change between surveys can be seen. The most recent survey is shown as a solid curve; the previous survey is dashed. The dates of the surveys are given to the right of the data; the lower date corresponds to the solid line.

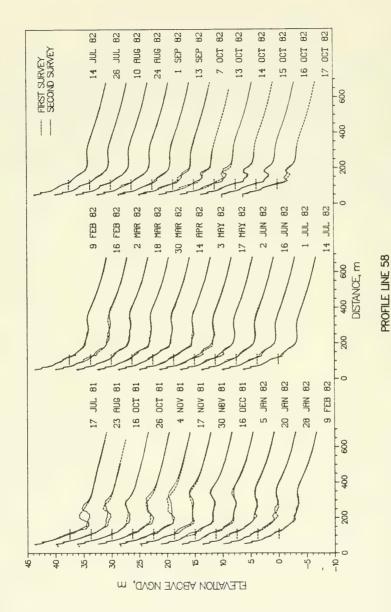


Figure Al. Profile line 58, 17 Jul 1981 - 17 Oct 1982

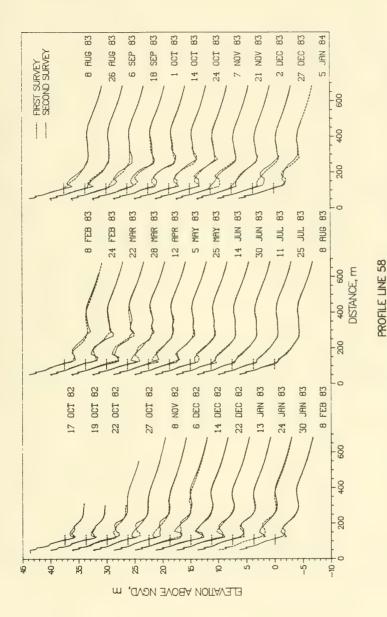


Figure A2. Profile line 58, 17 Oct 1982 - 5 Jan 1984

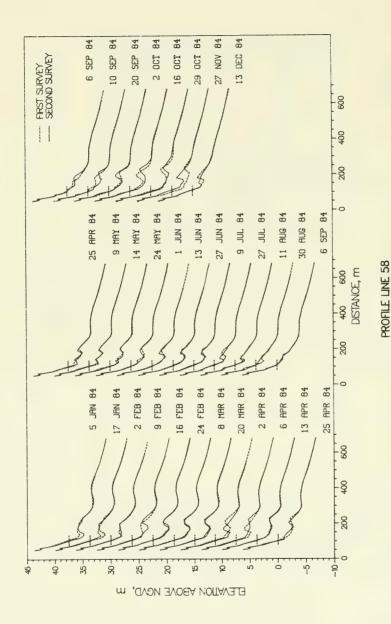


Figure A3. Profile line 58, 5 Jan 1984 - 13 Dec 1984

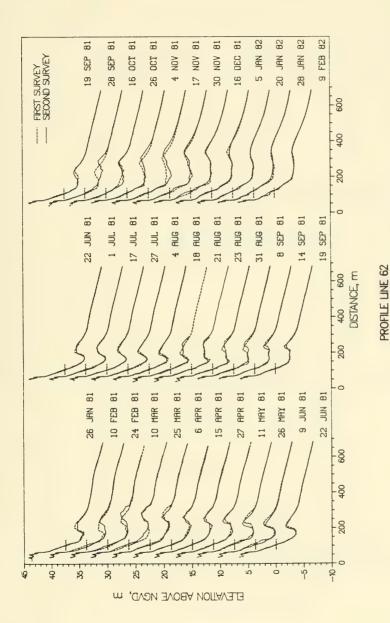


Figure A4. Profile line 62, 26 Jan 1981 - 9 Feb 1982

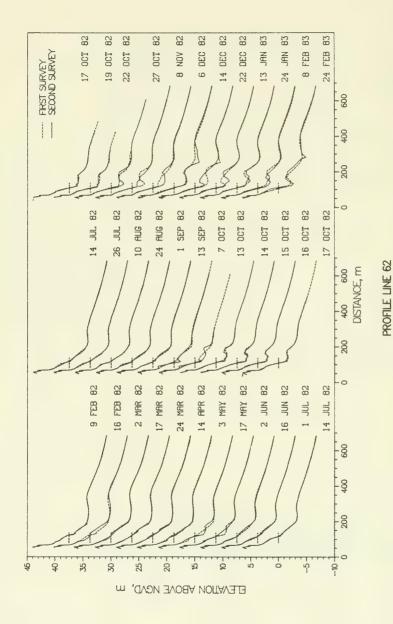


Figure A5. Profile line 62, 9 Feb 1982 - 24 Feb 1983

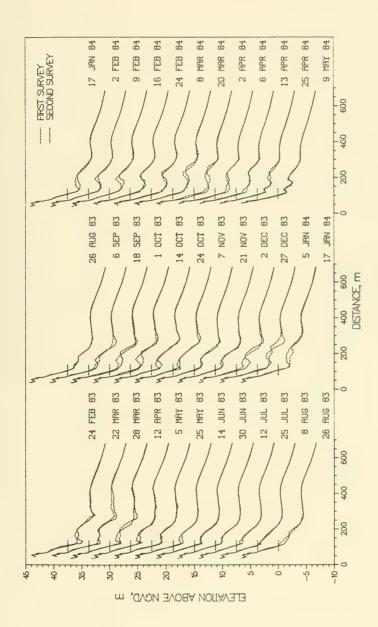


Figure A6. Profile line 62, 24 Feb 1983 - 9 May 1984

PROFILE LINE 62

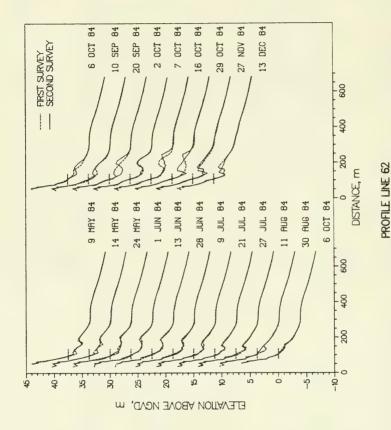


Figure A7. Profile line 62, 9 May 1984 - 13 Dec 1984

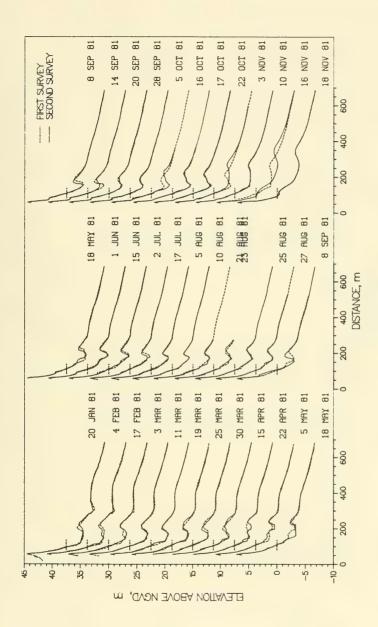


Figure A8. Profile line 188, 20 Jan 1981 - 18 Nov 1981

PROFILE LINE 188

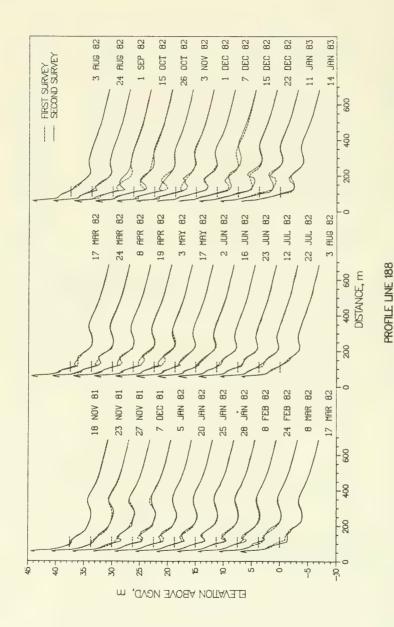


Figure A9. Profile line 188, 18 Nov 1981 - 14 Jan 1983

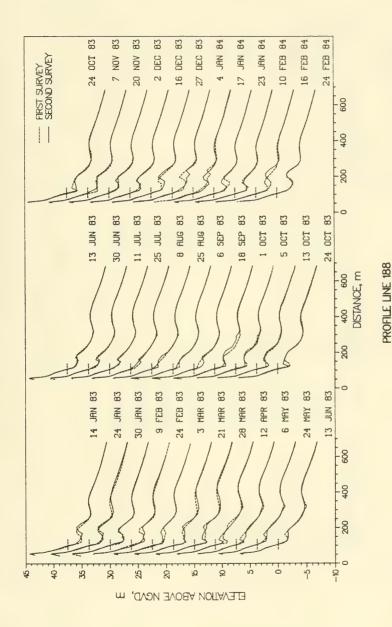


Figure AlO. Profile line 188, 14 Jan 1983 - 24 Feb 1984

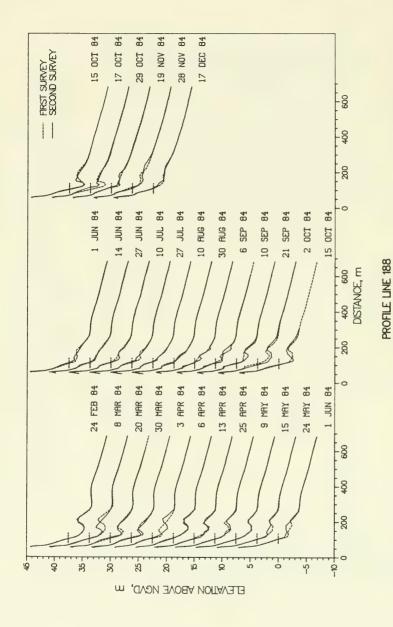


Figure All. Profile line 188, 24 Feb 1984 - 17 Dec 1984

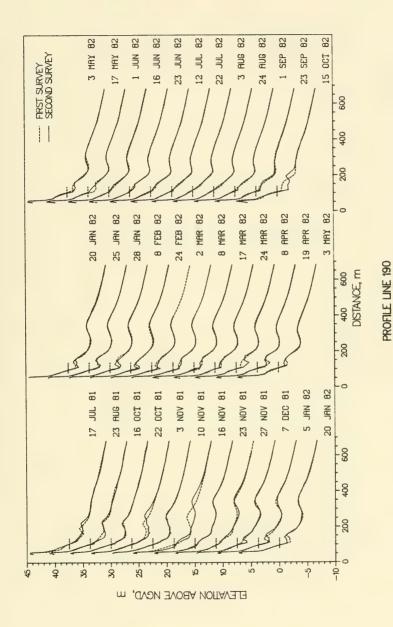


Figure Al2. Profile line 190, 17 Jul 1981 - 15 Oct 1982

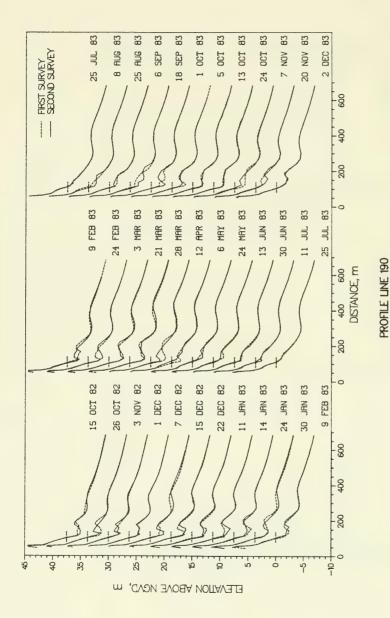


Figure A13. Profile line 190, 15 Oct 1982 - 2 Dec 1983

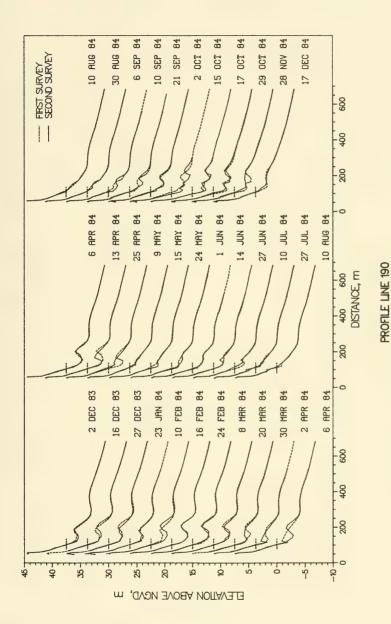


Figure Al4. Profile line 190, 2 Dec 1983 - 17 Dec 1984



#### APPENDIX B: SURVEY DATA LISTING

- 1. This appendix contains the profile data in BPAS Edit 2 card format (Fleming and DeWall 1982),\* along with a checksum value. When entering the data into a computer, do not enter any values past column 80. These are produced when the data are run through the program given in Appendix C. Use the given values to check your version for possible data-entry errors.
  - 2. The format of the data is as follows:

# First card in each record

| Position | Entry description                         | Format       |
|----------|---|--------------|
| 1-2      | Locality Code (ILOC)                      | A2           |
| 3-5      | Profile line number (IPROF)               | 13           |
| 6-9      | Survey identification number (ISUR)       | 14           |
| 10       | Card number (always 1 for first card) (N) | A1           |
| 11-16    | Date of survey (IDATE)                    | 16           |
| 17-21    | Time of survey (ITIME)                    | 15           |
| 22-24    | Number of coordinate pairs for survey (I) | 13           |
| 25-29    | Minimum elevation for survey (MIN)        | F5.2         |
| 30-40    | Data change codes (INFO)                  | A11          |
| 41-80    | First four distance-elevation pairs (Y,Z) | 4(F5.1,F5.2) |

### Continuation Cards

| 1-9   | Same as for first card         |              |
|-------|--------------------------------|--------------|
| 10    | Card number (2-9, then A-Z)    | A1           |
| 11-80 | Seven distance-elevation pairs | 7(F5.1.F5.2) |

If there are exactly four coordinate pairs (only one card needed), there must be a second blank card following.

3. The format statement to read the data is as follows:

```
READ (??,????) ILOC, IPROF, ISUR, N, IDATE, ITIME, I, MIN, .INFO, (Y(J), Z(J), J=1,I)

???? FORMAT (A2,I3,I4,A1,I6,I5,I3,F5.2,A11,4(F5.1,F5.2),/,(10X, .7(F5.1,F5.2)))
```

4. The correction codes contained in the INFO field have the following meanings:

| G =  | Gradual correction    | С | = | Constant correction    |
|------|-----------------------|---|---|------------------------|
| H =  | Horizontal correction | ٧ | = | Vertical correction    |
| D =  | Deletion of points    | Α | = | Addition of points     |
| Ë =  | Entire profile        | S | = | Selected random points |
| 0 =  | Offshore points       | В | = | Beach points           |
| MR = | Mini-Ranger data      |   |   |                        |

<sup>\*</sup> See References at the end of the main text.

The remaining space is used to give an indication of the magnitude of the changes made, either by the inclusion of the number of points affected or by the magnitude of the change, or both.

5. The survey data are shown in Table B1.

Table B1
Survey Data for Lines 58, 62, 188, and 190 for 1981-1984

| 39 58 | 291810717 1200 50-3200 1550 1980 1680 2050 1830 1690 1940 1540            | 56     |
|-------|---|--------|
| 39 58 | 292 2100 1530 2220 1340 2450 1040 2620 930 2750 800 2900 710 3080 590     | 0      |
| 39 58 | 293 3350 340 3390 370 3790 0 4090 -300 4390 -620 4620 -980 4890-1000      | 13     |
| 39 58 | 294 5050-1100 5240-1100 5720-1110 6090 -830 6430 -610 6830 -540 7260 -580 | 75     |
| 39 58 | 295 8190 -810 9040 -990 9670-112010510-125011700-135012740-141013880-1490 | 45     |
| 39 58 | 29615040-158016240-167017610-179019270-192021260-208022410-217023870-2260 | 15     |
| 39 58 | 29725670-239027100-247028460-254030200-265031490-273032950-280034210-2900 | 18     |
| 39 58 | 29835390-295036600-301037870-306039340-3200                               | 31     |
| 39 58 | 371810823 1600 43-2080 1690 2050 1810 1720 1940 1550 2140 1640            | 16     |
| 39 58 | 372 2240 1330 2400 1130 2490 1000 2840 630 3280 310 3620 -10 3820 -270    | 46 315 |
| 39 58 | 373 4080 -380 4310 -500 4660 -680 4900 -850 5130 -980 5440-1000 5680-1010 | 6      |
| 39 58 | 374 5910-1020 6080-1060 6360-1090 6630-1160 6980-1150 7260-1150 7510-1030 | 37     |
| 39 58 | 375 7750 -990 7970 -790 8330 -710 9080 -820 9610-104010030-113010460-1200 | 68     |
| 39 58 | 37611060-128011830-134012630-140013410-148014180-153015120-160016090-1670 | 42     |
| 39 58 | 37716840-175017900-184019320-194021000-2080                               | 73     |
| 39 58 | 461811016 1600 39-1760 1240 1910 1240 1940 1500 1960 1690 2020            | 99     |
| 39 58 | 462 1870 1620 2070 1560 2080 1590 2200 1410 2710 730 2820 620 3140 330    | 67     |
| 39 58 | 463 3400 90 3750 -150 4010 -360 4400 -540 4870 -760 5210 -850 5660 -890   | 26     |
| 39 58 | 464 5970 -870 6340 -900 6340 -900 6690 -940 7180 -970 7680 -970 8060 -930 | 54     |
| 39 58 | 465 8390 -900 8760 -860 9030 -830 9440 -830 9760 -86010110-101010390-1080 | 88 560 |
| 39 58 | 46610790-118011610-131012630-143013450-148014270-156014890-162016570-1760 | 13     |
| 39 58 | 491811026 1400 45-2380 1700 2030 1910 1580 2150 1570 2320 1200            | 52     |
| 39 58 | 492 2520 920 2770 670 2850 620 3020 460 3310 210 3570 20 3870 -280        | 9      |
| 39 58 | 493 4110 -380 4470 -530 4780 -680 5090 -760 5430 -850 5670-1020 5920-1020 | 88     |
| 39 58 | 494 6150-1060 6500-1070 6760-1030 7010-1070 7310-1080 7660 -960 7880 -960 | 36     |
| 39 58 | 495 8200 -900 8530 -860 8950 -790 9400 -810 9820 -92010490-110011210-1230 | 40     |
| 39 58 | 49612020-136012730-143013420-14901444C-157015450-167016570-176017550-1850 | 56     |
| 39 58 | 49718920-195020130-203021530-212022830-223023990-230025650-2380           | 99     |
| 39 58 | 501811104 1545 43-2920 1700 2010 1920 1570 2180 1460 2460 990             | 28     |
| 39 58 | 502 2680 740 2820 590 3060 420 3520 200 3900 -100 4040 -290 4420 -410     | 13 434 |
| 39 58 | 503 4950 -660 5200 -830 5480-1140 5720-1160 6090-1200 6450-1250 6860-1190 | 93     |
| 39 58 | 504 7280-1050 7710 -870 8160 -850 8790 -900 9460 -85010170 -80010860-1010 | 83     |
| 39 58 | 50511790-125012770-140013710-151014840-162016160-174017300-183018410-1900 | 51     |
| 39 58 | 50620220-205021950-217023450-228025000-237026630-246028140-254029880-2670 | 85     |
| 39 58 | 50731360-271032520-280033610-286034700-2920                               | 9      |
| 39 58 | 521811117 1330 48-2650 1280 1920 1550 1960 1690 1980 1700 2030            | 93     |
| 39 58 | 522 1810 1730 1920 1580 2030 1560 2140 1650 2210 1290 2360 1080 2510 910  | 79     |
| 39 58 | 523 2530 920 2820 760 3110 490 3500 140 3690 -200 3980 -320 4480 -520     | 53     |
| 39 58 | 524 4850 -720 5230 -990 5670-1170 6090-1180 6560-1110 7080-1090 7780-1090 | 35     |
| 39 58 | 525 8290-1080 8830-1060 9410-1040 9980 -97010690 -89011290 -94012040-1090 | 99 680 |
| 39 58 | 52612470-119013310-137014250-149015100-159016250-170017350-179018880-1920 | 77     |
| 39 58 | 52720820-208022020-217022850-222024140-231025380-239026740-246027880-2530 | 4      |
| 39 58 | 52829170-259030380-2650   | 82     |
| 39 58 | 551811130 1100 43-2540 1700 2020 1800 1760 1940 1570 2140 1530            | 87     |
|       |   |        |

(Sheet 1 of 61)

### Table Bl. (Continued)

```
58
39 58 552 2190 1300 2500 960 2570 900 2700 810 2800 770 3120 580 3340 230
39 58 553 3630 -40 4010 -120 4360 -210 4660 -360 4980 -600 5420 -940 5980-1090
                                                                                       39
39 58 554 6410-1070 6900-1080 7500-1070 8140-1110 8700-1130 9220-1160 9880-1120
                                                                                       99
39 58 55510520 -99011130 -89011710 -93012410-108013240-127013950-140014890-1540
                                                                                       70
       55615950-166017080-178018150-188019500-199020690-208021880-215023200-2250
                                                                                       96
       55724520-234025730-240026850-246027910-2540
                                                                                       73
                                                                                           685
39 58
                                        1705 2010 1867 1640 2069 1567 2148 1554
                                                                                       51
39 58
     571811216 1000 44-2626
      572 2192 1299 2380 1040 2671 862 2916 776 3069 624 3320 520 3724 334
                                                                                       34
39 58
      573 4043 -97 4163 -317 4464 -394 4779 -515 5179 -737 5554 -943 5904-1020
                                                                                       20
       574 6306-1049 6665-1045 7068-1042 7402-1040 7900-1073 8432-1120 9008-1195
                                                                                       90
39 58
       575 9621-118410336-103911079 -92111842 -98912637-113713463-130914385-1457
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39190 1493 5172 -500 5803 -606 6410 -742 7097 -953 7857-1149 8618-1247 9569-1273
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39190 149410801-130511935-134613212-144714305-155615790-174217167-185318491-1953
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39190 149519650-202620951-212822265-222923644-232224972-240826158-247627254-2541
                                                                                      15
                                                                                      75 452
39190 149628368-2603
39190 1501840601 110 30-2574 --- 1692 2386 1885 2282 2008 1582 2166 1262
                                                                                      5
39190 1502 2322 1056 2525 984 3068 356 3606 -329 3868 -356 4611 -576 5161 -659
                                                                                      51
39190 1503 5776 -627 6493 -726 7247 -982 8103-1202 9131-127210057-127911127-1293
39190 150412341-139113639-150514881-164616271-177117548-187919187-201620485-2122
                                                                                      51
39190 150521850-218623291-228124790-240726392-250827639-2574
                                                                                      18
                                       1699 2400 1887 2297 2042 1484 2492 998
                                                                                      38
39190 1511840614 1040 21-1833
39190 1512 2968 458 3352 86 3864 -389 4386 -554 5130 -617 5828 -603 6504 -750
39190 1513 7078 -953 7939-1178 8851-1253 9635-128710675-128911854-134313031-1445
                                                                                      97
39190 151414082-159015509-171816972-1833
                                                                                      34
                                        1701 2393 1888 2276 2044 1475 2289 1127
                                                                                      31 464
39190 1521840627 1035 32-2633
39190 1522 2564 958 3106 373 3670 -253 4077 -502 4520 -587 5021 -369 5829 -654
39190 1523 6187 -776 6681 -883 7228-1024 8022-1180 8871-1258 9848-126411106-1297
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39190 152521147-213322485-225023878-236125075-241026179-248127483-257729157-2633
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                                1695 2388 1885 2270 2017 1541 2426 1041
39190 1531840710 1045 29-2514
                                                                                      8
                                                                                      71
39190 1532 3016 479 3465 217 4000 -186 4558 -461 5069 -454 5744 -601 6460 -872
39190 1533 7140-1032 7944-1195 8501-1234 9036-1252 9935-126610897-131111713-1355
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                                                                                      57 384
39190 1551840727 1000 52-2521
39190 1552 2338 1078 2623 925 2940 537 3244 580 3562 116 3855 -262 4063 -295
                                                                                      87
39190 1553 4415 -289 4798 -418 5176 -531 5659 -682 6478 -881 6930-1005 7537-1128
                                                                                      88
                                                                                      17
39190 1554 7942-1194 8344-1222 8837-1247 9276-1253 9758-125710229-127410844-1290
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                                                                                       8
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                                                                                      16
                                                                                      AA
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                                       1705 2407 1887 2284 2020 1540 2378 1061
                                                                                      66
39190 1561840810 925 25-2425
39190 1562 2957 623 3387 348 3873 -75 4428 -279 4956 -476 5677 -724 6482 -894
39190 1563 7227-1066 7981-1197 8856-1254 9902-126111045-130412333-138313701-1514
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                                                                                      29
                                       1696 2397 1732 2438 1824 2340 1884 2280
                                                                                      89
39190 1571840830 1220 30-2459
39190 1572 2027 1525 2068 1413 2336 1104 2452 1025 2884 669 3418 161 3716 -34
39190 1573 4267 -163 4981 -369 5676 -723 6404 -912 7535-1140 8722-1248 9727-1263
                                                                                       នព
39190 157410487-128011717-133812819-144014009-155315390-169316690-180417986-1915
                                                                                      93
                                                                                       20
39190 157519805-204821358-217022909-228324156-236225864-2459
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39190 1581840906 1540 34-2518
39190 1582 2027 1525 2068 1413 2336 1074 2336 1104 2664 886 3118 390 3668 6
39190 1583 4266 -312 4721 -276 5358 -423 5829 -771 6475 -906 7272-1108 8109-1222
                                                                                       20
                                                                                       76
39190 1584 8942-1253 9801-126610915-129711978-136113147-144914363-159215783-1730
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39190 158517153-184817957-191719038-199220444-209821627-219022897-228124071-2355
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39190 158625473-244026729-2518
                                       1691 2385 1778 2385 1887 2264 1956 1823
                                                                                       9
39190 1591840910 1100 32-1966GH
39190 1592 2013 1534 2268 1087 2273 1131 2498 960 2549 977 2813 733 3124 445
                                                                                       95
39190 1593 3132 385 3330 262 3679 -247 4221 -454 4737 -534 5344 -422 5847 -476
                                                                                       90
39190 1594 6152 -614 6763 -961 7152-1076 7647-1174 8494-1233 9377-125210203-1277
39190 159510923-130412120-138313530-150515066-166616342-179517198-185718346-1966
                                                                                       7
                                        1703 2440 1807 2385 1892 2278 1951 1925
                                                                                       99
39190 1601840921 1045 30-2177
39190 1602 2050 1506 2184 1266 2331 1083 2495 1081 2619 927 2696 903 3099 507
                                                                                       43
39190 1603 3655 -100 4212 -402 4895 -753 5269 -782 5804 -584 6100 -545 6600 -699
                                                                                       26
39190 1604 7460-1037 8212-1187 9403-124910353-127111548-134512766-144713972-1559
                                                                                       87
                                                                                       62
39190 160515194-168316861-182618620-197020325-208621495-2177
                                        1601 2083 1696 2059 1815 2329 1890 2285
                                                                                       66
39190 1611841002 955 32-2553
39190 1612 2004 1617 2131 1312 2324 1118 2475 1043 2494 1002 2971 493 3451 53
                                                                                       43
39190 1613 3746 -324 4125 -385 4588 -747 5018 -791 5512 -748 6126 -538 6531 -562
                                                                                       27
39190 1614 7058 -797 7755-1051 8629-1202 9547-124410794-129511721-135012802-1473
                                                                                       11
39190 161514068-158615328-171218661-197220491-211523886-236025354-245626530-2553
                                                                                       92
                                        1694 2388 1743 2434 1835 2330 1893 2263
39190 1631841015 1000 33-1212
39190 1632 1935 2015 2033 1554 2081 1453 2157 1308 2318 1025 2478 857 2641 655
                                                                                       25
39190 1633 3031 169 3059 156 3500 -504 3788 -652 3902 -648 4155 -521 4510 -584
                                                                                       61
                                                                                           506
39190 1634 4854 -724 5193 -691 5221 -726 5868 -991 6117-1035 6413-1070 6644-1119
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39190 1635 6861 -920 7119 -807 7471 -771 7927 -856 8239 -946 8795-1082 9254-1175
                                                                                       1
                                                                                       37
39190 1636 9766-1212
                                                                                       21
39190 1641841017 1445 39-2370GV
                                       1694 2388 1743 2434 1835 2330 1893 2263
39190 1642 1935 2015 2033 1554 2081 1453 2157 1308 2353 936 2478 859 2684 593
                                                                                       84
39190 1643 3109 109 3504 -502 3807 -791 4043 -788 4326 -716 4751 -612 5163 -557
                                                                                       65
```

(Sheet 60 of 61)

# Table B1. (Concluded)

| 39190 1644 5592 -858 6121-1050 6592 -923 7463 -726 7915 -840  | 8576-1021 9095-1116 80     |  |
|---|----------------------------|--|
| 39190 1645 9932-121310730-126411962-137712787-143413826-1554  | 14896-165016408-1782 42    |  |
| 39190 164617403-187618810-200220045-209720967-216922035-2233  | 23131-229324233-2370 97    |  |
| 39190 1651841029 1220 40-2841 1651 2263 1682 2404             | 1735 2462 1882 2285 46 569 |  |
| 39190 1652 1930 2002 2021 1573 2164 1271 2379 911 2748 610    | 3308 75 3746 -538 7        |  |
| 39190 1653 3920 -641 4322 -741 4698 -642 5099 -658 5404 -966  | 5606 -936 5971 -982 42     |  |
| 39190 1654 6295 -919 6772 -719 7458 -645 8084 -801 9024-10213 | 10200-118211383-1298 30    |  |
| 39190 165512562-142013700-155414833-167116253-180917885-1936  | 19268-204920701-2152 46    |  |
| 39190 165622464-226723696-234825248-243126775-251727932-25862 |                            |  |
| 39190 165732073-2841  | 76                         |  |
| 39190 1671841128 1030 46-2319D02 1646 2248 1689 2388          |                            |  |
| 39190 1672 1884 2243 2016 1563 2152 1295 2282 1093 2323 1015  |                            |  |
|   | 3585 ~147 3800 -264 82     |  |
| 39190 1674 4103 -478 4119 -492 4343 -632 4524 -685 4720 -678  |                            |  |
| 39190 1675 5556 -637 5874 -596 6225 -614 6697 -630 7107 -649  |                            |  |
| 39190 1676 9086-104210111-118811044-128711983-138913139-15181 |                            |  |
| 39190 167716284-183017401-190318758-201019810-208720716-21532 |                            |  |
| 39190 1681841217 1315 44-2549 1884 2278 2034 1539             |                            |  |
|   | 3846 -217 4159 -306 5      |  |
| 39190 1683 4679 -559 5250 -653 5881 -643 6578 -654 7093 -711  |                            |  |
|   |                            |  |
| 39190 1684 9488-108010340-119111217-131111969-139212758-1485  |                            |  |
| 39190 168515147-171916162-181616755-186317412-191018101-1971  |                            |  |
| 39190 168620318-213220909-217621583-221022205-225322817-2297  |                            |  |
| 39190 168725139-243325779-247326347-249026895-254926895-2529  | 16 467                     |  |



#### APPENDIX C: PROGRAM DATACHECK

The following program was written as an aid to the proper entry of the profile data into the user's computer system. The program was run on the correct data at the Field Research Facility and the proper checksum values added to the BPAS format file as explained in Appendix B. The data should be entered without the checksum values and then run through this program. Compare the checksum values with those given in Appendix B. The code was developed on a Control Data Corporation computer, but should be easily converted to any system running an implementation of FORTRAN 77.

PROGRAM DATCHK (INPUT, OUTPUT, TAPE7)

C

```
C
              AUTHOR: MS. REBECCA SAVAGE, WESCD-F
  THIS PROGRAM IS DESIGNED FOR THE DATA PROCESSER TO COMPARE COPIES
C
C
   OF DATA FILES TO MAKE SURE TRANSFERED COPIES ARE CORRECT.
C
   THE COPY CAN BE CHECKED AT EVERY LINE OR EVERY TEN LINES.
C
C
  THE PROGRAM READS FROM FORTRAN UNIT 7 AND WRITES TO UNIT 8
C
       INTEGER*2 ICARD(25), ITOT, LTOT, I, J, N, V, STOT
       CHARACTER*1 LINE(80), CARD(25)
C
       DATA ICARD/1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,
                   20,21,22,23,24,25/
       DATA CARD/'.',' ','-','0','1','2','3','4','5','6','7','8','9',
                  'G', 'H', 'D', 'E', 'O', 'M', 'R', 'C', 'V', 'A', 'S', 'B'/
C
C
   DATA IS READ IN LINE BY LINE
C
       N=1
       V=1
       STOT=0
      ITOT=0
       READ(7,100,END=99) LINE
  100
      FORMAT(80A1)
C
   ASSIGN INTEGER VALUES TO CHARACTER DATA
C
C
   AND KEEP SUMS OF DATA BASED ON CHARACTER AND LOCATION IN LINE
C
       DO 10, I=1,80
          DO 20, J=1,25
           IF (LINE(I).EQ.CARD(J))THEN
             ITOT=ICARD(J)*I+ITOT
             GO TO 10
           END IF
   20
          CONTINUE
          WRITE (*,103) LINE(I),N,I
```

```
WRITE(8,103) LINE(I),N,I
         FORMAT('UNKNOWN CHARACTER ',A1,' IN LINE', 15,' AT COLUMN', 13)
  103
  10 CONTINUE
CC
C REDUCE THE SUMS TO A MANAGABLE LEVEL, KEEP A LINE SUM (LTOT)
C AND A SUM OF TEN LTOT VALUES (STOT). N COUNTS THE LINE NUMBER IN
C THE DATA FILE, V COUNTS THE TEN LINE INCREMENT FOR STOT.
C EACH LINE IS OUTPUT WITH ITS VALUE OF LTOT. EACH TENTH LINE
C ALSO INCLUDES STOT
     LTOT=MOD(ITOT, 100)
      STOT=LTOT+STOT
      N=N+1
      IF(V.EQ.10)THEN
        WRITE(8,101) LINE, LTOT, STOT
  101
        FORMAT(80A1,5X,215)
        V=1
        STOT=0
       ELSE
        WRITE (8,102) LINE, LTOT
  102
       FORMAT(80A1,5X,15)
        V=V+1
      END IF
      GO TO 50
   99 STOP
      END
```

### APPENDIX D: WAVE HEIGHTS AT PIER END, 1981-1984

This Appendix presents plots (Figures D1 to D4) of significant wave height at the pier end for each of the 4 years of this report, 1981-1984. The data from the pier-end Baylor wave staff have been combined with transformed data from the nearshore Waverider buoy to provide as complete a record as possible. It should be noted that the pier-end location becomes saturated with respect to wave height at approximately 2.8 m; thus, a value of 2.8 m may indicate that the significant wave height is greater farther offshore.

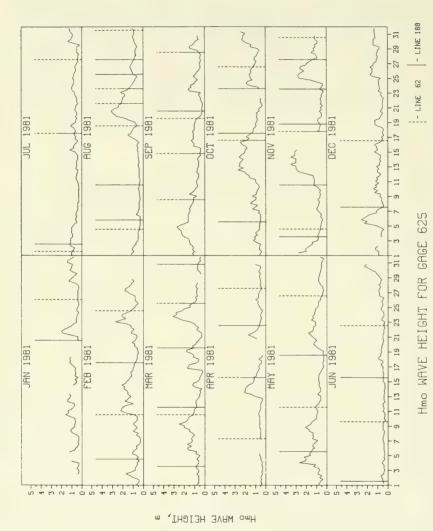


Figure D1. Wave height at pier end and times of surveys of lines 62 and 188, 1981

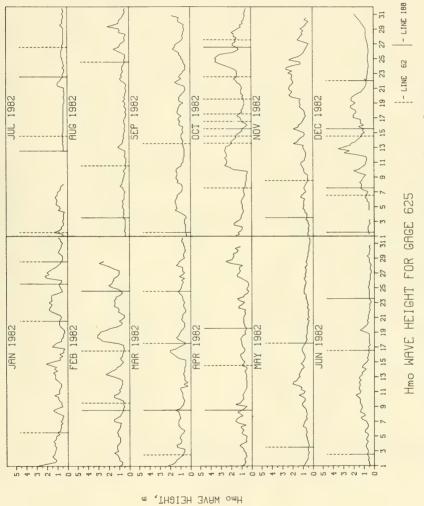
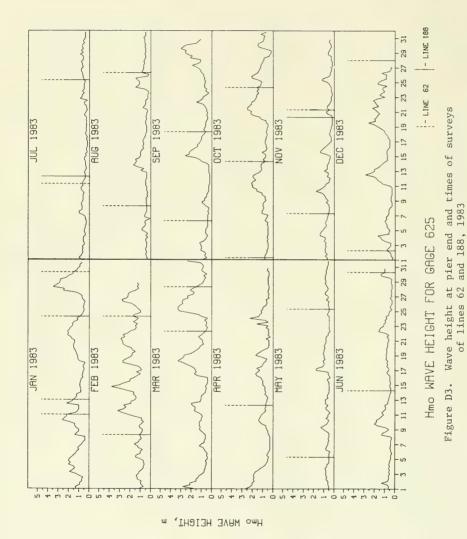


Figure D2. Wave height at pier end and times of surveys of lines 62 and 188, 1982



D4

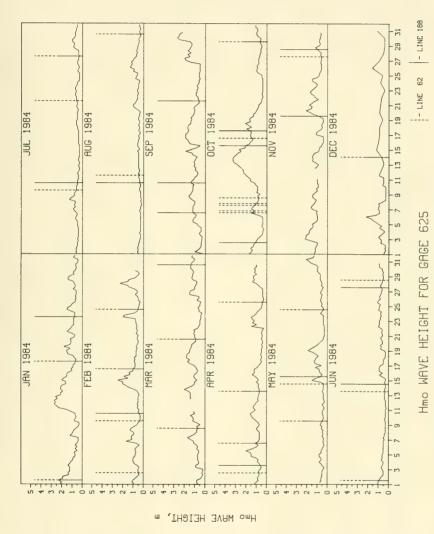


Figure D4. Wave height at pier end and times of surveys of lines 62 and 188, 1984



Table El lists wave height and peak period for the 4 years covered by this report (1981-1984). The wave heights contained in the table are equivalent to those presented graphically in Appendix D. The periods are the period associated with the maximum energy peak in the wave spectrum calculated from a discrete Fourier transform of the record. Details of these calculations can be found in the main text.

Table El
Wave Data From 1981-1984

|        |           | JANUARY 1981 |            |        |            | FEBRUARY 1981 |            |
|--------|-----------|--------------|------------|--------|------------|---------------|------------|
|        |           |              |            |        |            |               |            |
| DAY    | TIME      | PERIOD (S)   | HEIGHT (M) | DAY    | TIME       | PERIOD (S)    | HEIGHT (M) |
| 1      | 0         | 10.0         | 1.1        | 1      | 100        | 8.0           | 0.7        |
| 2      | 1200      | 10.0         | 0.4        | 2      | 100        | 7.0           | 1.0        |
| 3      | 0         | 10.0         | 0.3        | 3      | 100        | 10.0          | 0.8        |
| 4      | 0<br>1200 | 6.0<br>6.0   | 0.3        | 4      | 100        | 9.0           | 0.6        |
| 5<br>6 | 100       | 6.0          | 1.2<br>0.6 | 5<br>6 | 100        | 12.5          | 0.7        |
| 7      | 100       | 12.0         | 0.3        | 7      | 100        | 6.0           | 0.6        |
| 8      | 115       | 5.0          | 0.9        | 8      | 100        | 14.0          | 0.3        |
| 9      | 100       | 7.0          | 0.9        | 9      | 100        | 12.0          | 0.5        |
| 10     | 105       | 4.0          | 0.7        | 10     | 100<br>700 | 8.0           | 8.0        |
| 11     | 105       | 5.0          | 1.4        | 11     | 100        | 10.3<br>9.0   | 0.6        |
| 12     | 105       | 4.0          | 0.8        | 11     | 700        | 9.0           | 2.2        |
| 13     | 105       | 6.0          | 1.1        | 11     | 1300       | 9.0           | 2.0        |
| 14     | 1310      | 12.0         | 0.8        | 12     | 100        | 9.0           | 1.0        |
| 15     | 105       | 10.0         | 0.5        | 13     | 100        | 7.0           | 1.2        |
| 16     | 100       | 4.0          | 0.6        | 14     | 100        | 9.0           | 1.9        |
| 17     | 1300      | 7.0          | 1.2        | 14     | 1300       | 12.0          | 2.1        |
| 18     | 100       | 7.0          | 1.2        | 15     | 100        | 10.0          | 1.6        |
| 20     | 1300      | 10.3         | 0.4        | 16     | 100        | 12.0          | 1.2        |
| 21     | 100       | 9.1          | 0.4        | 17     | 100        | 10.0          | 0.9        |
| 21     | 1900      | 8.0          | 2.0        | 18     | 100        | 9.0           | 0.6        |
| 22     | 100       | 9.0          | 1.7        | 19     | 100        | 9.0           | 0.5        |
| 23     | 100       | 9.0          | 0.5        | 20     | 100        | 7.0           | 0.8        |
| 24     | 100       | 5.0          | 0.4        | 21     | 100        | 8.0           | 0.6        |
| 25     | 100       | 3.0          | 0.4        | 22     | 100        | 9.0           | 0.9        |
| 26     | 100       | 6.0          | 0.4        | 23     | 100        | 12.0          | 2.7        |
| 27     | 100       | 10.8         | 0.4        | 23     | 700        | 14.0          | 2.2        |
| 28     | 100       | 5.4          | 0.4        | 23     | 1905       | 16.0          | 2.1        |
| 29     | 100       | 5.9          | 0.9        | 24     | 105        | 14.0          | 2.0        |
| 30     | 100       | 5.0          | 1.2        | 25     | 100        | 14.0          | 0.8        |
| 31     | 100       | 5.0          | 1.4        | 26     | 100        | 5.0           | 0.8        |
|        |           |              |            | 27     | 100        | 10.0          | 1.5        |
|        |           |              |            |        |            |               |            |

(Continued)

(Sheet 1 of 22)

|          |              |              |            | 28       | 100          | 10.0         | 1.2        |
|----------|--------------|--------------|------------|----------|--------------|--------------|------------|
|          |              | MARCH 1981   |            |          |              | APRIL 1981   |            |
| DAY      | TIME         | PERIOD (S)   | HEIGHT (M) | DAY      | TIME         | PERIOD (S)   | HEIGHT (M) |
| 1        | 100          | 12.0         | 0.8        | 1        | 100          | 8.0          | 0.4        |
| 2        | 100          | 10.0         | 0.6        | 2        | 100          | 6.0          | 0.5        |
| 3        | 115          | 10.0         | 0.6        | 3        | 100          | 8.0          | 0.3        |
| 4        | 100          | 5.0          | 0.6        | 4        | 100          | 14.0         | 0.3        |
| 5        | 100          | 7.0          | 0.5        | 5        | 100          | 6.0          | 0.6        |
| 6        | 100          | 16.0         | 1.7        | 7        | 700          | 9.0          | 0.6        |
| 7        | 100          | 10.0         | 1.2        | 8        | 100          | 9.0          | 0.5        |
| 8        | 100          | 12.0         | 1.2        | 9        | 1900         | 12.0<br>11.0 | 0.6<br>0.6 |
| 8        | 1900         | 14.0         | 2.0        | 10       | 100          |              |            |
| 9        | 100          | 14.0         | 2.0        | 11       | 100          | 10.0         | 0.6<br>0.5 |
| 9        | 700          | 14.0         | 2.5        | 12       | 100          | 10.0         | 1.1        |
| 10       | 100          | 14.0         | 1.6        | 13       | 100          | 5.0          | 2.1        |
| 11       | 815          | 12.0         | 1.0        | 13       | 1300<br>1900 | 10.0<br>11.0 | 2.0        |
| 12       | 700          | 12.0         | 0.9        | 13<br>14 | 100          | 11.0         | 2.0        |
| 13       | 100          | 14.0         | 0.5        | 15       | 100          | 10.0         | 1.2        |
| 14       | 100          | 12.0         | 0.3        |          | 100          | 7.0          | 0.9        |
| 15       | 100          | 6.0          | 0.7        | 16       |              | 8.5          | 0.7        |
| 16       | 100          | 9.0          | 0.3        | 17       | 100          | 6.4          | 0.7        |
| 17       | 100          | 6.0          | 1.6        | 18       | 100          | 5.0          | 0.9        |
| 18       | 110          | 12.0         | 0.6        | 20<br>21 | 1900         | 6.0          | 1.3        |
| 19       | 100          | 6.0          | 1.8        |          | 100          | 8.0          | 0.8        |
| 20       | 100          | 7.0          | 0.9        | 22<br>23 | 100          | 9.0          | 0.5        |
| 21       | 100          | 9.0          | 0.3        | 24       | 100          | 16.0         | 0.5        |
| 22       | 100          | 5.0          | 0.8        | 25       | 1300         | 13.7         | 0.8        |
| 23       | 100          | 12.0         | 1.4        | 26       | 100          | 5.1          | 1.0        |
| 23       | 700          | 14.0         | 2.2        | 27       | 100          | 12.8         | 0.6        |
| 23       | 1302         | 7.0          | 3.1        | 28       | 100          | 12.1         | 0.5        |
| 23       | 1900         | 8.0          | 2.7        | 29       | 100          | 3.8          | 0.6        |
| 24<br>24 | 100          | 10.0<br>12.0 | 2.8        | 30       | 100          | 7.0          | 0.6        |
| 24       | 700          | 12.0         | 2.2        | 30       | 100          | ,            | 0.0        |
| 24       | 1300<br>1905 | 12.0         | 2.0        |          |              |              |            |
| 25       | 117          | 12.0         | 1.4        |          |              |              |            |
| 26       | 100          | 10.0         | 0.8        |          |              |              |            |
| 27       | 100          | 10.0         | 0.8        |          |              |              |            |
| 28       | 100          | 3.0          | 0.8        |          |              |              |            |
|          |              | 14.0         | 0.4        |          |              |              |            |
| 29       | 1300         | 14.0         | 0.4        |          |              |              |            |
| 30       | 100          | 7.0          | 0.6        |          |              |              |            |
| 31       | 100          | 7.0          | 0.0        |          |              |              |            |

|        |            | MAY 1981   |            |        |      | JUNE 1981   |                   |
|--------|------------|------------|------------|--------|------|-------------|-------------------|
| DAY    | TIME       | PERIOD (S) | HEIGHT (M) | DAY    | TIME | PERIOD (S)  | HEIGHT (M)        |
| 1      | 100        | 5.0        | 0.8        | 1      | 700  | 8.0         | 0.4               |
| 2      | 100        | 3.0        | 0.7        | 2      | 100  | 4.0         | 0.6               |
| 3      | 100        | 5.0        | 0.7        | 3      | 100  | 8.0         | 0.3               |
| 4      | 100        | 10.0       | 2.7        | 4      | 100  | 9.0         | 0.6               |
| 4      | 700        | 9.0        | 2.1        | 5      | 705  | 9.0         | 0.3               |
| 4      | 1300       | 11.3       | 2.0        | 6      | 100  | 9.1         | 0.4               |
| 4      | 1900       | 12.0       | 2.2        | 7      | 100  | 8.0         | 0.5               |
| 5      | 100        | 10.0       | 1.6        | 8      | 100  | 8.0         | 0.4               |
| 6      | 105        | 10.0       | 1.2        | 9      | 100  | 9.0         | 0.5               |
| 7      | 100        | 8.0        | 0.9        | 10     | 100  | 9.0         | 0.4               |
| 8      | 115        | 5.0        | 1.3        | 11     | 105  | 8.0         | 0.5               |
| 8      | 1900       | 7.0        | 2.1        | 12     | 100  | 8.0         | 0.5               |
| 9      | 100        | 8.0        | 1.8        | 13     | 100  | 8.0         | 0.4               |
| 10     | 100        | 8.0        | 1.0        | 14     | 100  | 8.0         | 0.3               |
| 11     | 100        | 8.0        | 0.9        | 15     | 100  | 8.0         | 0.5               |
| 12     | 100        | 6.0        | 0.8        | 16     | 100  | 10.0        | 0.4               |
| 13     | 100        | 8.0        | 0.6        | 17     | 100  | 9.0         | 0.5               |
| 14     | 105        | 9.0        | 0.6        | 18     | 100  | 4.0         | 0.9               |
| 15     | 100        | 10.0       | 0.8        | 19     | 100  | 8.0         | 0.6               |
| 16     | 1300       | 8.0        | 0.5        | 20     | 100  | 9.0         | 0.5               |
| 17     | 100        | 8.0        | 0.3        | 21     | 710  | 8.0         | 0.5               |
| 18     | 100        | 7.0        | 0.3        | 22     | 100  | 6.0         | 0.4               |
| 19     | 100        | 8.0        | 0.3        | 23     | 100  | 6.0         | 0.3               |
| 20     | 100        | 6.0        | 1.3        | 24     | 100  | 3.0         | 0.4               |
| 21     | 700        | 5.0        | 1.6        | 25     | 100  | 5.0         | 0.6               |
| 22     | 100        | 8.0        | 1.3        | 26     | 700  | 10.7        | 0.4               |
| 23     | 100        | 10.0       | 1.1        | 27     | 700  | 4.7         | 0.9               |
| 24     | 100        | 10.0       | 1.2        | 28     | 100  | 5.7         | 0.9               |
| 25     | 100        | 10.0       | 0.9        | 29     | 100  | 5.3         | 0.8               |
| 26     | 100        | 9.0        | 0.6        | 30     | 100  | 10.5        | 1.6               |
| 27     | 100        | 9.0        | 0.4        | 30     | 1300 | 11.5        | 2.3               |
| 28     | 100        | 6.0        | 0.6        | 30     | 1900 | 7.7         | 2.1               |
| 29     | 100        | 8.0        | 0.8        |        |      |             |                   |
| 30     | 100        | 8.0        | 0.6        |        |      |             |                   |
| 31     | 100        | 7.0        | 0.5        |        |      |             |                   |
|        |            |            |            |        |      |             |                   |
|        |            | JULY 1981  |            |        |      | AUGUST 1981 |                   |
| DA     | Y TIME     | PERIOD (S) | HEIGHT (M) | DAY    | TIME | PERIOD (S)  | HEIGHT (M)        |
| 1      | 100        | 10.6       | 1.0        | 1      | 100  | 6.0         | 1.2               |
| 2      | 100        | 7.9        | 0.7        | 2      | 100  | 7.0         | 1.0               |
| _      |            |            |            |        |      |             |                   |
| 3      | 100        | 8.2        | 1.1        | 3      | 100  | 7.0         | 0.5               |
| 3<br>4 | 100<br>100 | 8.2<br>7.6 | 1.1        | 3<br>4 | 100  | 7.0<br>9.1  | 0.5<br>0.5<br>0.3 |

| 6  | 100  | 8.4  | 0.6 | 6   | 100  | 9.0  | 0.3 |
|----|------|------|-----|-----|------|------|-----|
| 7  | 700  | 8.8  | 0.4 | 7   | 100  | 5.0  | 0.5 |
| 8  | 100  | 8.7  | 0.4 | 8   | 100  | 10.0 | 0.4 |
| 9  | 100  | 9.9  | 0.3 | 9   | 1300 | 7.0  | 0.4 |
| 10 | 100  | 10.0 | 0.3 | 10  | 100  | 9.0  | 0.5 |
| 11 | 1300 | 3.7  | 0.6 | 11  | 705  | 10.0 | 0.3 |
| 12 | 100  | 9.6  | 0.5 | 12  | 700  | 10.0 | 0.4 |
| 13 | 100  | 9.6  | 0.5 | 13  | 100  | 10.0 | 0.5 |
| 14 | 100  | 9.1  | 0.4 | 14  | 700  | 12.0 | 0.5 |
| 15 | 100  | 3.2  | 0.7 | 15  | 100  | 11.0 | 0.5 |
| 16 | 100  | 6.1  | 0.7 | 16  | 100  | 10.5 | 0.6 |
| 17 | 100  | 10.6 | 0.6 | 17  | 715  | 5.0  | 1.5 |
| 18 | 100  | 4.4  | 0.7 | 18  | 700  | 6.0  | 0.9 |
| 19 | 100  | 8.7  | 0.6 | 19  | 100  | 4.0  | 0.8 |
| 20 | 100  | 8.3  | 0.5 | 19  | 2000 | 8.0  | 2.6 |
| 21 | 100  | 6.4  | 0.6 | 20  | 200  | 9.0  | 2.8 |
| 22 | 700  | 6.6  | 0.5 | 20  | 800  | 9.0  | 3.0 |
| 23 | 100  | 8.4  | 0.7 | 20  | 1400 | 11.0 | 3.1 |
| 24 | 100  | 8.3  | 0.9 | 20  | 2000 | 10.0 | 2.8 |
| 25 | 100  | 6.8  | 0.9 | 21  | 200  | 11.0 | 2.4 |
| 26 | 100  | 7.7  | 0.6 | 21  | 800  | 12.0 | 2.4 |
| 27 | 100  | 8.2  | 0.5 | 21  | 1400 | 12.0 | 2.1 |
| 28 | 100  | 6.6  | 0.4 | 21  | 2000 | 12.0 | 2.1 |
| 29 | 100  | 2.1  | 0.5 | 22  | 200  | 12.0 | 2.0 |
| 30 | 100  | 6.0  | 1.4 | 22  | 800  | 11.0 | 2.0 |
| 31 | 100  | 4.0  | 0.9 | 23  | 200  | 12.0 | 2.2 |
|    |      |      |     | 24  | 710  | 11.0 | 1.0 |
|    |      |      |     | 25  | 700  | 12.0 | 0.6 |
|    |      |      |     | 2.6 | 700  | 6.0  | 1.2 |
|    |      |      |     | 27  | 700  | 8.0  | 1.0 |
|    |      |      |     | 28  | 700  | 9.0  | 0.7 |
|    |      |      |     | 29  | 100  | 8.0  | 0.7 |
|    |      |      |     | 30  | 100  | 6.0  | 0.9 |
|    |      |      |     | 31  | 100  | 7.0  | 0.9 |
|    |      |      |     |     |      |      |     |

### SEPTEMBER 1981

# OCTOBER 1981

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 100  | 8.3        | 1.1        | 1   | 100  | 12.0       | 0.6        |
| 2   | 100  | 9.0        | 1.1        | 2   | 100  | 12.0       | 0.6        |
| 3   | 100  | 10.0       | 1.5        | 3   | 100  | 6.8        | 1.2        |
| 3   | 1300 | 12.0       | 2.0        | 4   | 100  | 6.0        | 1.0        |
| 3   | 1900 | 12.0       | 2.2        | 5   | 100  | 8.9        | 0.6        |
| 4   | 800  | 14.0       | 2.3        | 6   | 100  | 11.3       | 0.5        |
| 4   | 1400 | 12.0       | 2.5        | 7   | 100  | 3.6        | 0.6        |
| 4   | 2000 | 12.0       | 2.7        | 8   | 100  | 5.7        | 1.5        |
| 5   | 200  | 14.0       | 2.4        | 9   | 100  | 6.0        | 1.3        |
| 6   | 1300 | 11.9       | 1.6        | 10  | 100  | 6.0        | 0.7        |

(Continued)

(Sheet 4 of 22)

| 7  | 100 | 12.5 | 1.4 | 11 | 100  | 5.0  | 1.0 |
|----|-----|------|-----|----|------|------|-----|
| 8  | 700 | 11.4 | 1.1 | 12 | 100  | 6.0  | 1.9 |
| 9  | 100 | 10.8 | 0.8 | 12 | 700  | 6.0  | 2.0 |
| 10 | 100 | 10.2 | 0.9 | 12 | 1400 | 7.0  | 2.7 |
| 11 | 100 | 12.5 | 0.8 | 12 | 2000 | 7.0  | 2.2 |
| 12 | 100 | 11.4 | 0.6 | 13 | 200  | 8.0  | 2.6 |
| 13 | 100 | 10.2 | 0.6 | 13 | 900  | 8.0  | 2.5 |
| 14 | 100 | 11.8 | 0.7 | 13 | 1400 | 6.0  | 2.5 |
| 15 | 100 | 12.0 | 0.4 | 13 | 2000 | 6.0  | 2.3 |
| 16 | 200 | 14.0 | 1.0 | 14 | 100  | 8.1  | 2.2 |
| 17 | 700 | 8.0  | 1.1 | 14 | 700  | 9.4  | 2.6 |
| 18 | 100 | 12.0 | 1.0 | 14 | 1400 | 10.0 | 2.4 |
| 19 | 100 | 11.0 | 0.9 | 14 | 2000 | 9.0  | 2.1 |
| 20 | 100 | 7.0  | 0.3 | 15 | 200  | 10.0 | 2.0 |
| 21 | 800 | 8.0  | 0.2 | 15 | 800  | 11.0 | 2.0 |
| 22 | 100 | 11.0 | 0.4 | 15 | 1909 | 11.0 | 2.0 |
| 23 | 100 | 9.0  | 0.4 | 16 | 109  | 12.0 | 2.3 |
| 24 | 100 | 7.0  | 1.4 | 16 | 807  | 12.0 | 2.5 |
| 25 | 100 | 6.0  | 0.9 | 17 | 200  | 11.0 | 1.9 |
| 26 | 100 | 6.0  | 0.6 | 18 | 100  | 12.0 | 1.2 |
| 27 | 100 | 10.0 | 0.5 | 19 | 700  | 10.0 | 0.8 |
| 28 | 100 | 9.0  | 0.4 | 20 | 100  | 5.0  | 0.8 |
| 29 | 100 | 6.0  | 1.4 | 21 | 100  | 9.1  | 0.5 |
| 30 | 100 | 14.0 | 0.9 | 22 | 100  | 8.3  | 0.5 |
|    |     |      |     | 23 | 1400 | 7.0  | 0.7 |
|    |     |      |     | 24 | 100  | 5.0  | 1.6 |
|    |     |      |     | 25 | 100  | 5.0  | 1.5 |
|    |     |      |     | 26 | 100  | 7.0  | 1.5 |
|    |     |      |     | 27 | 100  | 10.0 | 1.0 |
|    |     |      |     | 28 | 100  | 6.7  | 0.9 |
|    |     |      |     | 29 | 100  | 4.0  | 0.8 |
|    |     |      |     | 30 | 200  | 9.0  | 2.2 |
|    |     |      |     | 30 | 700  | 8.0  | 2.3 |
|    |     |      |     | 30 | 1400 | 6.0  | 2.2 |
|    |     |      |     | 30 | 1935 | 7.0  | 2.2 |
|    |     |      |     | 31 | 200  | 7.0  | 2.0 |
|    |     |      |     | 31 | 800  | 9.0  | 2.4 |

NOVEMBER 1981

## DECEMBER 1981

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 900  | 12.0       | 2.7        | 1   | 100  | 7.0        | 0.9        |
| 1   | 1400 | 12.0       | 2.0        | 2.  | 100  | 10.0       | 1.2        |
| 1   | 2000 | 12.0       | 2.1        | 3   | 1300 | 9.0        | 0.6        |
| 2   | 200  | 12.0       | 1.9        | 4   | 100  | 6.0        | 0.6        |
| 3   | 100  | 11.0       | 0.9        | 5   | 100  | 5.0        | 1.1        |
| 4   | 719  | 10.0       | 0.7        | 5   | 900  | 10.0       | 2.3        |
| 5   | 1405 | 7.0        | 0.5        | 5   | 1400 | 11.0       | 2.0        |

(Continued)

(Sheet 5 of 22)

| 6  | 805  | 6.0  | 0.6 | 5  | 2000 | 12.0 | 2.6 |
|----|------|------|-----|----|------|------|-----|
| 7  | 700  | 7.0  | 1.0 | 6  | 200  | 12.0 | 2.3 |
| 8  | 700  | 11.0 | 0.7 | 6  | 800  | 12.0 | 2.0 |
| 9  | 700  | 14.0 | 0.6 | 7  | 100  | 11.1 | 1.1 |
| 10 | 700  | 4.0  | 0.9 | 8  | 100  | 12.3 | 0.5 |
| 11 | 700  | 4.0  | 1.2 | 9  | 100  | 5.0  | 0.8 |
| 12 | 800  | 7.0  | 2.7 | 10 | 100  | 7.0  | 1.4 |
| 12 | 1400 | 8.0  | 2.9 | 11 | 100  | 7.1  | 1.2 |
| 12 | 2000 | 9.0  | 3.0 | 12 | 100  | 6.0  | 0.7 |
| 13 | 200  | 10.0 | 3.0 | 13 | 100  | 7.0  | 1.1 |
| 13 | 800  | 12.0 | 3.5 | 14 | 100  | 9.0  | 0.8 |
| 13 | 1400 | 10.0 | 3.0 | 15 | 100  | 9.0  | 1.3 |
| 14 | 200  | 14.0 | 3.0 | 16 | 100  | 10.9 | 1.3 |
| 14 | 800  | 12.0 | 3.5 | 17 | 100  | 9.9  | 0.6 |
| 14 | 1340 | 12.0 | 3.1 | 18 | 100  | 9.0  | 0.4 |
| 14 | 2000 | 11.0 | 3.1 | 19 | 100  | 6.0  | 1.2 |
| 15 | 200  | 12.0 | 3.1 | 20 | 100  | 6.0  | 0.6 |
| 15 | 700  | 12.0 | 2.9 | 21 | 100  | 6.0  | 0.5 |
| 17 | 1900 | 5.6  | 0.9 | 22 | 100  | 9.4  | 0.5 |
| 18 | 100  | 7.0  | 0.7 | 23 | 100  | 6.4  | 0.6 |
| 19 | 100  | 4.0  | 0.8 | 24 | 1300 | 5.3  | 0.9 |
| 20 | 100  | 3.5  | 0.5 | 25 | 100  | 5.1  | 0.7 |
| 21 | 100  | 4.0  | 0.6 | 26 | 200  | 6.0  | 1.5 |
| 22 | 100  | 4.0  | 0.6 | 27 | 100  | 6.0  | 1.4 |
| 23 | 100  | 4.0  | 0.4 | 28 | 100  | 8.0  | 1.0 |
| 24 | 100  | 12.0 | 0.4 | 29 | 100  | 9.7  | 0.8 |
| 25 | 100  | 8.0  | 2.7 | 30 | 100  | 5.7  | 1.4 |
| 25 | 800  | 9.0  | 2.8 | 31 | 700  | 4.7  | 1.3 |
| 25 | 1400 | 12.0 | 2.7 |    |      |      |     |
| 25 | 1900 | 13.7 | 2.5 |    |      |      |     |
| 26 | 100  | 13.1 | 2.2 |    |      |      |     |
| 26 | 800  | 12.0 | 2.6 |    |      |      |     |
| 26 | 1500 | 14.0 | 2.5 |    |      |      |     |
| 26 | 2000 | 14.0 | 2.0 |    |      |      |     |
| 27 | 200  | 17.0 | 1.9 |    |      |      |     |
| 28 | 100  | 14.0 | 1.0 |    |      |      |     |
| 29 | 100  | 6.0  | 1.3 |    |      |      |     |
| 30 | 100  | 4.0  | 0.9 |    |      |      |     |
|    |      |      |     |    |      |      |     |

# JANUARY 1982

### FEBRUARY 1982

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 100  | 10.0       | 2.9        | 1   | 100  | 8.0        | 0.9        |
| 1   | 700  | 11.0       | 2.1        | 2   | 100  | 5.0        | 1.0        |
| 2   | 100  | 10.0       | 1.3        | 3   | 100  | 7.0        | 1.1        |
| 3   | 1300 | 6.0        | 1.1        | 4   | 100  | 8.0        | 1.0        |
| 4   | 100  | 7.0        | 1.2        | 5   | 200  | 10.0       | 1.1        |
| 5   | 100  | 10.2       | 1.1        | 6   | 100  | 11.0       | 1.0        |

(Continued)

(Sheet 6 of 22)

| 6  | 100  | 12.6 | 0.7 | 7  | 100  | 5.0  | 1.5 |
|----|------|------|-----|----|------|------|-----|
| 7  | 100  | 14.0 | 0.7 | 8  | 100  | 10.0 | 0.8 |
| 8  | 900  | 6.0  | 1.3 | 9  | 100  | 11.0 | 0.5 |
| 9  | 100  | 14.0 | 0.5 | 10 | 100  | 4.0  | 1.0 |
| 10 | 100  | 6.0  | 0.9 | 11 | 100  | 10.0 | 0.9 |
| 11 | 100  | 2.8  | 0.8 | 12 | 100  | 8.0  | 0.7 |
| 12 | 100  | 4.4  | 0.6 | 13 | 100  | 6.0  | 1.5 |
| 13 | 800  | 6.0  | 1.2 | 13 | 900  | 7.0  | 2.3 |
| 14 | 200  | 10.0 | 1.3 | 13 | 1400 | 8.0  | 2.0 |
| 14 | 1900 | 6.2  | 2.1 | 14 | 200  | 9.0  | 1.3 |
| 15 | 100  | 7.5  | 1.5 | 15 | 100  | 10.0 | 0.6 |
| 16 | 200  | 10.0 | 0.8 | 16 | 100  | 11.0 | 0.7 |
| 17 | 200  | 6.0  | 1.5 | 17 | 100  | 7.0  | 0.6 |
| 18 | 200  | 4.0  | 0.6 | 17 | 2000 | 10.0 | 2.6 |
| 19 | 100  | 11.0 | 0.3 | 18 | 200  | 12.0 | 2.8 |
| 20 | 100  | 6.0  | 0.8 | 18 | 800  | 11.0 | 3.1 |
| 21 | 100  | 5.0  | 0.6 | 18 | 1400 | 11.0 | 3.1 |
| 22 | 200  | 7.0  | 1.8 | 18 | 2000 | 12.0 | 2.9 |
| 23 | 100  | 7.0  | 1.8 | 19 | 200  | 11.0 | 2.8 |
| 24 | 100  | 10.6 | 1.5 | 19 | 200  | 11.0 | 2.8 |
| 25 | 100  | 4.0  | 0.7 | 19 | 800  | 11.0 | 2.2 |
| 26 | 100  | 8.4  | 0.6 | 20 | 100  | 11.0 | 0.8 |
| 26 | 800  | 6.0  | 2.0 | 21 | 100  | 7.0  | 0.5 |
| 26 | 1400 | 7.0  | 2.2 | 22 | 100  | 10.0 | 1.0 |
| 27 | 200  | 7.0  | 2.0 | 23 | 200  | 9.0  | 1.4 |
| 28 | 200  | 8.0  | 0.9 | 24 | 100  | 10.0 | 0.9 |
| 29 | 100  | 12.0 | 0.5 | 25 | 200  | 6.0  | 1.7 |
| 30 | 100  | 12.0 | 0.8 | 25 | 800  | 7.0  | 2.0 |
| 31 | 100  | 5.0  | 0.5 | 26 | 200  | 6.0  | 1.5 |
|    |      |      |     | 27 | 200  | 11.0 | 1.0 |
|    |      |      |     | 27 | 2300 | 7.0  | 2.1 |
|    |      |      |     | 28 | 800  | 9.0  | 2.9 |
|    |      |      |     | 28 | 1400 | 10.0 | 2.5 |
|    |      |      |     | 29 | 2000 | 11.0 | 2.6 |
|    |      |      |     |    |      |      |     |

MARCH 1982

APRIL 1982

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 200  | 11.0       | 2.2        | 1   | 100  | 9.0        | 0.9        |
| 2   | 903  | 10.0       | 0.9        | 2   | 100  | 10.0       | 0.7        |
| 3   | 100  | 8.0        | 0.6        | 3   | 100  | 10.0       | 0.8        |
| 4   | 200  | 6.0        | 1.0        | 4   | 100  | 6.0        | 0.9        |
| 5   | 705  | 8.0        | 0.9        | 5   | 100  | 10.0       | 0.5        |
| 6   | 100  | 3.0        | 0.9        | 6   | 200  | 5.0        | 1.0        |
| 7   | 200  | 10.0       | 1.2        | 7   | 100  | 7.0        | 1.6        |
| 8   | 800  | 6.0        | 1.2        | 8   | 700  | 6.0        | 1.4        |
| 9   | 100  | 8.0        | 0.9        | 9   | 100  | 5.0        | 0.5        |
| 10  | 730  | 5.0        | 0.8        | 10  | 100  | 7.0        | 0.8        |

| 11 | 100  | 9.0  | 0.9 | 11 | 1300 | 8.0  | 0.5 |
|----|------|------|-----|----|------|------|-----|
| 12 | 100  | 11.0 | 0.7 | 12 | 100  | 11.0 | 0.5 |
| 13 | 100  | 12.0 | 0.6 | 13 | 100  | 4.0  | 0.5 |
| 14 | 100  | 11.0 | 0.6 | 14 | 100  | 7.0  | 0.5 |
| 15 | 100  | 11.0 | 0.5 | 15 | 100  | 6.0  | 0.7 |
| 16 | 900  | 8.0  | 2.0 | 16 | 100  | 5.0  | 1.1 |
| 16 | 1400 | 8.0  | 2.0 | 17 | 100  | 7.0  | 0.9 |
| 17 | 200  | 10.0 | 1.1 | 18 | 100  | 7.0  | 1.1 |
| 18 | 100  | 5.0  | 1.2 | 19 | 100  | 7.0  | 0.7 |
| 19 | 100  | 9.0  | 1.0 | 20 | 100  | 7.0  | 0.7 |
| 20 | 100  | 8.0  | 0.6 | 21 | 100  | .7.0 | 0.8 |
| 21 | 100  | 5.0  | 0.8 | 22 | 100  | 8.0  | 0.6 |
| 22 | 100  | 11.0 | 0.5 | 23 | 100  | 7.0  | 0.7 |
| 23 | 100  | 11.0 | 0.6 | 24 | 100  | 9.0  | 0.7 |
| 24 | 100  | 4.0  | 0.9 | 25 | 100  | 10.0 | 0.4 |
| 25 | 100  | 7.0  | 0.9 | 26 | 100  | 6.0  | 0.7 |
| 26 | 100  | 7.0  | 0.9 | 27 | 100  | 10.0 | 1.2 |
| 27 | 100  | 9.0  | 0.6 | 28 | 100  | 10.0 | 0.9 |
| 28 | 100  | 7.0  | 1.4 | 28 | 824  | 6.0  | 2.1 |
| 29 | 100  | 7.0  | 0.6 | 28 | 1400 | 7.0  | 2.5 |
| 30 | 100  | 9.0  | 0.5 | 29 | 205  | 9.0  | 1.8 |
| 31 | 100  | 9.0  | 0.7 | 30 | 200  | 8.0  | 1.3 |

#### MAY 1982

# JUNE 1982

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 100  | 11.0       | 0.9        | 1   | 100  | 14.0       | 0.4        |
| 2   | 100  | 10.0       | 0.5        | 2   | 100  | 9.0        | 0.5        |
| 3   | 100  | 9.0        | 0.5        | 3   | 100  | 7.0        | 0.6        |
| 4   | 100  | 10.0       | 0.5        | 4   | 100  | 6.0        | 0.7        |
| 5   | 100  | 5.0        | 0.7        | 5   | 100  | 5.0        | 0.6        |
| 6   | 201  | 9.0        | 0.7        | 6   | 100  | 8.0        | 0.7        |
| 7   | 200  | 9.0        | 0.8        | 7   | 100  | 8.0        | 0.8        |
| 8   | 100  | 10.0       | 0.6        | 8   | 100  | 9.0        | 1.0        |
| 9   | 100  | 11.0       | 1.0        | 9   | 100  | 9.0        | 1.2        |
| 10  | 100  | 11.0       | 0.8        | 10  | 100  | 10.0       | 1.4        |
| 11  | 100  | 11.0       | 0.8        | 11  | 100  | 12.0       | 1.3        |
| 12  | 100  | 14.0       | 2.0        | 12  | 100  | 11.0       | 1.4        |
| 13  | 100  | 12.0       | 1.3        | 13  | 100  | 11.0       | 1.4        |
| 14  | 100  | 11.0       | 1.1        | 14  | 100  | 11.0       | 0.8        |
| 15  | 100  | 10.0       | 1.0        | 15  | 100  | 9.0        | 0.7        |
| 16  | 100  | 9.0        | 0.9        | 16  | 100  | 9.0        | 0.6        |
| 17  | 100  | 11.0       | 1.0        | 17  | 100  | 10.0       | 0.6        |
| 18  | 100  | 9.0        | 0.6        | 18  | 100  | 14.0       | 0.5        |
| 19  | 100  | 9.0        | 0.6        | 19  | 100  | 7.0        | 0.9        |
| 20  | 100  | 9.0        | 0.5        | 20  | 100  | 10.0       | 0.7        |
| 21  | 100  | 9.0        | 0.4        | 21  | 100  | 10.0       | 0.6        |
| 22  | 100  | 8.0        | 0.4        | 22  | 100  | 9.0        | 0.4        |

| 23 | 100 | 7.0  | 0.6 | 23 | 100 | 10.0 | 0.3 |
|----|-----|------|-----|----|-----|------|-----|
| 24 | 100 | 7.0  | 0.7 | 24 | 100 | 8.0  | 0.5 |
| 25 | 100 | 9.0  | 0.8 | 25 | 100 | 7.0  | 0.6 |
| 26 | 100 | 9.0  | 0.8 | 26 | 100 | 11.0 | 0.4 |
| 27 | 100 | 10.0 | 0.7 | 27 | 100 | 7.0  | 0.3 |
| 28 | 100 | 9.0  | 0.6 | 28 | 100 | 8.0  | 0.3 |
| 29 | 100 | 9.0  | 0.6 | 29 | 100 | 6.0  | 0.5 |
| 30 | 100 | 9.0  | 0.4 | 30 | 700 | 8.0  | 0.4 |
| 31 | 100 | 10.0 | 0.3 |    |     |      |     |

| JULY | 1982 | AUGUS | T 1982 |
|------|------|-------|--------|
|      |      |       |        |

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 100  | 10.0       | 0.4        | 1   | 100  | 14.0       | 0.4        |
| 2   | 100  | 5.0        | 0.6        | 2   | 100  | 12.0       | 0.4        |
| 3   | 100  | 6.0        | 0.5        | 3   | 100  | 12.0       | 0.4        |
| 4   | 100  | 5.0        | 0.4        | 4   | 100  | 11.0       | 0.5        |
| 5   | 100  | 6.0        | 0.8        | 5   | 100  | 10.0       | 0.7        |
| 6   | 100  | 7.0        | 1.1        | 6   | 100  | 8.0        | 0.5        |
| 7   | 100  | 6.0        | 0.9        | 7   | 100  | 9.0        | 0.4        |
| 8   | 100  | 9.0        | 0.4        | 8   | 105  | 6.0        | 0.7        |
| 12  | 1300 | 8.0        | 0.4        | 9   | 100  | 9.0        | 0.5        |
| 13  | 100  | 11.0       | 0 - 4      | 10  | 700  | 8.0        | 0.3        |
| 14  | 100  | 11.0       | 0.5        | 11  | 100  | 8.0        | 0.3        |
| 15  | 100  | 10.0       | 0.4        | 12  | 100  | 7.0        | 0.4        |
| 16  | 100  | 10.0       | 0.4        | 13  | 100  | 6.0        | 1.1        |
| 17  | 100  | 7.0        | 0.4        | 14  | 100  | 6.0        | 0.6        |
| 18  | 100  | 11.0       | 0.4        | 15  | 100  | 6.0        | 0.5        |
| 19  | 100  | 9.0        | 0.3        | 16  | 100  | 6.0        | 0.4        |
| 20  | 100  | 7.0        | 0.3        | 17  | 100  | 7.0        | 0.4        |
| 21  | 100  | 2.0        | 0.3        | 18  | 100  | 8.0        | 0.3        |
| 22  | 100  | 7.0        | 0.7        | 19  | 100  | 10.0       | 0.4        |
| 23  | 100  | 10.0       | 0.4        | 20  | 100  | 6.0        | 0.4        |
| 24  | 100  | 7.0        | 0.3        | 21  | 100  | 6.0        | 0.4        |
| 25  | 100  | 4.0        | 0.5        | 22  | 100  | 4.0        | 0.8        |
| 26  | 100  | 10.0       | 0.6        | 23  | 100  | 6.0        | 0.7        |
| 27  | 100  | 8.0        | 0.4        | 24  | 100  | 6.0        | 0.6        |
| 28  | 100  | 9.0        | 0.4        | 25  | 100  | 10.0       | 0.4        |
| 29  | 100  | 7.0        | 0.4        | 26  | 737  | 6.0        | 1.5        |
| 30  | 100  | 7.0        | 0.5        | 27  | 100  | 6.0        | 0.8        |
| 31  | 100  | 9.0        | 0.5        | 28  | 100  | 9.0        | 0.4        |
|     |      |            |            | 29  | 100  | 6.0        | 1.0        |
|     |      |            |            | 29  | 800  | 6.0        | 2.1        |
|     |      |            |            | 30  | 100  | 7.0        | 1.0        |
|     |      |            |            | 31  | 100  | 8.0        | 0.5        |

|          | 5          | SEPTEMBER 1982 | 2          |          |            | OCTOBER 1982 |            |
|----------|------------|----------------|------------|----------|------------|--------------|------------|
| DAY      | TIME       | PERIOD (S)     | HEIGHT (M) | DAY      | TIME       | PERIOD (S)   | HEIGHT (M) |
| 1        | 100        | 8.0            | 0.4        | 1        | 100        | 7.0          | 1.6        |
| 2        | 100        | 6.0            | 0.5        | 2        | 100        | 10.0         | 0.9        |
| 3        | 100        | 7.0            | 0.6        | 3        | 100        | 7.0          | 1.4        |
| 4        | 100        | 9.0            | 0.8        | 4        | 100        | 9.0          | 0.9        |
| 5        | 100        | 6.0            | 1.4        | 5        | 100        | 11.0         | 0.9        |
| 6        | 700        | 6.0            | 1.3        | 6        | 100        | 14.0         | 0.9        |
| 7        | 100        | 6.0            | 0.9        | 7        | 100        | 11.0         | 0.8        |
| 8        | 100        | 4.0            | 0.9        | 8        | 100        | 8.0          | 0.6        |
| 9        | 100        | 10.0           | 1.4        | 9        | 100        | 9.0          | 0.5        |
| 10       | 100        | 11.0           | 1.4        | 10       | 100        | 6.0          | 1.8        |
| 11       | 100        | 10.0           | 0.7        | 10       | 800        | 8.0          | 2.1        |
| 12       | 100        | 8.0            | 0.6        | 10       | 1415       | 12.0         | 2.6        |
| 13       | 100        | 6.0            | 0.7        | 10       | 2000       | 14.0         | 2.4        |
| 14       | 100        | 6.0            | 0.8        | 11       | 200        | 14.0         | 2.4        |
| 15       | 100        | 6.0            | 0.7        | 11       | 800        | 14.0         | 2.4        |
| 16       | 100        | 10.0           | 1.1        | 11       | 1403       | 14.0         | 2.6        |
| 17       | 100        | 11.0           | 1.1        | 11       | 2000       | 14.0         | 2.4        |
| 18       | 100        | 10.0           | 1.2        | 12       | 200        | 14.0         | 2.4        |
| 19       | 100        | 11.0           | 0.7        | 12       | 700        | 17.0         | 2.5        |
| 20       | 710        | 6.0            | 0.8        | 12       | 1500       | 17.0         | 2.6        |
| 21       | 100        | 8.0            | 0.5        | 12       | 2000       | 12.0         | 2.5        |
| 22       | 100        | 6.0            | 1.2<br>0.8 | 13       | 200<br>800 | 14.0<br>17.0 | 2.1        |
| 23       | 100        | 8.0            |            | 13<br>13 | 1900       | 12.0         | 2.0        |
| 24       | 100<br>100 | 11.0<br>9.0    | 0.5        | 13       | 822        | 14.0         | 1.5        |
| 25<br>26 | 100        | 5.0            | 1.4        | 15       | 100        | 12.0         | 1.1        |
| 27       | 100        | 8.0            | 1.3        | 16       | 100        | 11.0         | 0.4        |
| 28       | 100        | 8.0            | 0.8        | 17       | 100        | 6.0          | 1.1        |
| 29       | 100        | 9.0            | 0.6        | 18       | 100        | 14.0         | 1.0        |
| 30       | 100        | 6.0            | 1.2        | 19       | 100        | 14.0         | 0.7        |
|          | 200        |                |            | 20       | 100        | 6.0          | 0.8        |
|          |            |                |            | 21       | 100        | 7.0          | 0.9        |
|          |            |                |            | 22       | 100        | 10.0         | 1.5        |
|          |            |                |            | 23       | 100        | 5.0          | 1.4        |
|          |            |                |            | 23       | 2000       | 6.0          | 2.1        |
|          |            |                |            | 24       | 200        | 7.0          | 2.6        |
|          |            |                |            | 24       | 800        | 8.0          | 3.1        |
|          |            |                |            | 24       | 1400       | 10.0         | 3.5        |
|          |            |                |            | 24       | 2000       | 12.0         | 3.4        |
|          |            |                |            | 25       | 200        | 14.0         | 3.5        |
|          |            |                |            | 25       | 800        | 14.0         | 3.3        |
|          |            |                |            | 25       | 1400       | 12.0         | 3.0        |
|          |            |                |            | 26       | 200        | 12.0         | 1.4        |
|          |            |                |            | 27       | 100        | 10.0         | 1.8        |
|          |            |                |            | 28       | 100        | 12.0         | 1.7        |
|          |            |                |            | 29       | 100        | 12.0         | 1.3        |

| 30 | 100 | 11.0 | 0.9 |
|----|-----|------|-----|
| 31 | 100 | 10.0 | 0.7 |

# NOVEMBER 1982

#### DECEMBER 1982

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 100  | 17.0       | 0.5        | 1   | 800  | 10.0       | 0.5        |
| 2   | 100  | 17.0       | 0.5        | 2   | 100  | 5.0        | 0.6        |
| 3   | 100  | 6.0        | 0.5        | 3   | 100  | 9.0        | 0.5        |
| 4   | 100  | 7.0        | 0.6        | 4   | 1300 | 10.0       | 0.5        |
| 5   | 100  | 6.0        | 0.9        | 5   | 100  | 10.0       | 0.5        |
| 6   | 100  | 8.0        | 0.8        | 6   | 100  | 12.0       | 0.7        |
| 7   | 100  | 7.0        | 0.7        | 7   | 100  | 11.0       | 0.6        |
| 8   | 100  | 9.0        | 0.7        | 8   | 100  | 6.0        | 1.2        |
| 9   | 700  | 11.0       | 0.5        | 9   | 100  | 6.0        | 1.0        |
| 10  | 100  | 5.0        | 0.9        | 9   | 2100 | 6.0        | 2.0        |
| 11  | 100  | 7.0        | 1.1        | 10  | 100  | 7.0        | 1.5        |
| 12  | 100  | 8.0        | 0.7        | 11  | 107  | 10.0       | 0.8        |
| 13  | 100  | 7.0        | 1.0        | 12  | 107  | 6.0        | 1.7        |
| 14  | 100  | 6.0        | 1.4        | 12  | 700  | 7.0        | 2.9        |
| 15  | 100  | 10.0       | 0.9        | 12  | 1400 | 11.0       | 2.4        |
| 16  | 100  | 6.0        | 1.4        | 12  | 2000 | 11.0       | 3.5        |
| 17  | 100  | 11.0       | 0.8        | 13  | 800  | 11.0       | 2.3        |
| 18  | 100  | 9.0        | 0.9        | 13  | 1400 | 12.0       | 2.2        |
| 19  | 100  | 7.0        | 1.3        | 14  | 1300 | 12.0       | 1.2        |
| 19  | 2000 | 8.0        | 2.1        | 15  | 100  | 12.0       | 0.9        |
| 20  | 200  | 8.0        | 2.3        | 16  | 100  | 7.0        | 1.0        |
| 20  | 800  | 10.0       | 2.1        | 17  | 100  | 6.0        | 2.0        |
| 20  | 1300 | 11.0       | 2.0        | 17  | 817  | 7.0        | 2.0        |
| 20  | 2000 | 12.0       | 2.3        | 18  | 100  | 6.0        | 1.8        |
| 21  | 200  | 12.0       | 2.3        | 18  | 800  | 7.0        | 2.2        |
| 21  | 800  | 12.0       | 2.2        | 18  | 1400 | 8.0        | 2.3        |
| 21  | 1400 | 12.0       | 2.0        | 18  | 2000 | 11.0       | 2.0        |
| 22  | 200  | 12.0       | 2.0        | 19  | 100  | 11.0       | 1.8        |
| 22  | 800  | 14.0       | 2.1        | 19  | 800  | 14.0       | 2.2        |
| 22  | 1500 | 14.0       | 2.0        | 19  | 1400 | 12.0       | 2.2        |
| 22  | 2000 | 14.0       | 2.0        | 19  | 2000 | 14.0       | 2.1        |
| 23  | 200  | 14.0       | 2.4        | 20  | 100  | 14.0       | 1.9        |
| 23  | 800  | 11.0       | 2.0        | 21  | 100  | 12.0       | 0.9        |
| 23  | 1400 | 14.0       | 2.6        | 22  | 700  | 17.0       | 0.9        |
| 23  | 2000 | 14.0       | 2.5        | 23  | 100  | 16.8       | 0.6        |
| 24  | 200  | 12.0       | 1.9        | 24  | 100  | 15.8       | 0.5        |
| 24  | 2000 | 7.0        | 2.3        | 25  | 100  | 14.0       | 0.6        |
| 25  | 100  | 6.0        | 2.0        | 26  | 100  | 15.3       | 0.5        |
| 26  | 100  | 6.0        | 0.8        | 27  | 100  | 7.8        | 0.6        |
| 27  | 100  | 10.0       | 0.4        | 28  | 100  | 5.7        | 0.8        |
| 28  | 100  | 7.0        | 1.2        | 29  | 100  | 6.3        | 0.8        |
| 29  | 100  | 6.0        | 1.2        | 30  | 100  | 4.9        | 1.3        |

30 100 7.0 0.4 31 100 5.5 1.9

|     |            | JANUARY 1983 |            |     | Ę    | EBRUARY 1983 |            |
|-----|------------|--------------|------------|-----|------|--------------|------------|
|     |            | DED (C)      | HEICHT (M) | DAY | TIME | PERIOD (S)   | HEIGHT (M) |
| DAY | 100        | PERIOD (S)   | HEIGHT (M) | 1   | 100  | 11.0         | 1.1        |
| 1   |            | 11.0<br>10.0 | 0.7        | 2   | 100  | 5.0          | 0.9        |
| 2   | 100<br>100 | 5.0          | 1.3        | 3   | 100  | 9.0          | 1.2        |
| 4   | 100        | 6.0          | 1.5        | 4   | 100  | 9.0          | 0.7        |
| 4   | 700        | 6.0          | 2.0        | 5   | 100  | 5.0          | 1.0        |
| 4   | 1900       | 7.0          | 2.0        | 6   | 100  | 8.0          | 1.0        |
| 5   | 100        | 9.0          | 1.9        | 7   | 100  | 9.0          | 1.6        |
| 6   | 100        | 7.0          | 1.2        | 8   | 100  | 11.0         | 1.0        |
| 7   | 100        | 9.0          | 0.7        | 9   | 100  | 12.0         | 0.8        |
| 8   | 100        | 9.0          | 0.4        | 10  | 100  | 6.0          | 0.7        |
| 9   | 100        | 4.0          | 1.0        | 11  | 100  | 6.0          | 2.2        |
| 10  | 100        | 7.0          | 1.9        | 11  | 700  | 8.0          | 2.8        |
| 10  | 700        | 10.0         | 2.6        | 11  | 1300 | 10.0         | 3.2        |
| 10  | 1300       | 10.0         | 2.4        | 11  | 1900 | 11.0         | 2.6        |
| 10  | 1900       | 10.0         | 2.2        | 12  | 100  | 12.0         | 2.4        |
| 11  | 100        | 10.0         | 2.1        | 12  | 700  | 12.0         | 2.6        |
| 12  | 100        | 10.0         | 1.0        | 13  | 100  | 12.0         | 1.5        |
| 12  | 1300       | 7.0          | 2.2        | 14  | 100  | 6.0          | 1.6        |
| 13  | 100        | 11.0         | 1.5        | 14  | 700  | 8.0          | 2.3        |
| 14  | 100        | 11.0         | 0.8        | 14  | 1300 | 10.0         | 3.0        |
| 15  | 100        | 14.0         | 0.9        | 14  | 1900 | 12.0         | 3.8        |
| 16  | 100        | 11.0         | 0.6        | 15  | 100  | 12.0         | 3.0        |
| 17  | 100        | 12.0         | 0.5        | 15  | 700  | 11.0         | 2.6        |
| 18  | 100        | 12.0         | 0.4        | 15  | 1300 | 12.0         | 2.0        |
| 19  | 1300       | 6.0          | 1.3        | 15  | 1900 | 12.0         | 2.0        |
| 20  | 100        | 8.0          | 1.5        | 16  | 100  | 11.0         | 1.6        |
| 21  | 100        | 6.0          | 1.4        | 17  | 100  | 12.0         | 0.9        |
| 21  | 1900       | 7.0          | 2.1        | 18  | 100  | 8.0          | 2.7        |
| 22  | 100        | 7.0          | 2.0        | 18  | 700  | 10.0         | 2.7        |
| 22  | 700        | 7.0          | 2.1        | 18  | 1300 | 11.0         | 2.4        |
| 23  | 100        | 9.0          | 1.6        | 18  | 1900 | 11.0         | 2.0        |
| 24  | 100        | 10.0         | 1.2        | 19  | 100  | 11.0         | 1.8        |
| 25  | 100        | 9.0          | 0.5        | 20  | 100  | 11.0         | 1.9        |
| 26  | 100        | 9.0          | 0.5        | 20  | 700  | 15.0         | 2.4        |
| 27  | 100        | 8.0          | 0.7        | 20  | 1300 | 15.0         | 2.7        |
| 27  | 1900       | 8.0          | 2.5        | 20  | 1900 | 16.0         | 2.7        |
| 28  | 100        | 9.0          | 2.4        | 21  | 100  | 15.0         | 2.8        |
| 28  | 700        | 11.0         | 3.5        | 21  | 700  | 13.0         | 2.9        |
| 28  | 1300       | 9.0          | 3.2        | 21  | 1300 | 15.0         | 2.5        |
| 28  | 1900       | 14.0         | 2.9        | 21  | 1900 | 14.0         | 2.7        |
| 29  | 100        | 12.0         | 2.8        | 22  | 100  | 14.0         | 2.2        |
| 29  | 700        | 12.0         | 2.8        | 22  | 700  | 13.0         | 2.0        |
| 29  | 1300       | 12.0         | 2.2        | 23  | 100  | 13.0         | 1.5        |

| 29 | 1900 | 12.0 | 2.0 | 24 | 100  | 13.0 | 1.2 |
|----|------|------|-----|----|------|------|-----|
| 30 | 100  | 12.0 | 1.6 | 25 | 100  | 12.0 | 1.0 |
| 31 | 100  | 11.0 | 0.9 | 26 | 100  | 10.0 | 1.9 |
|    |      |      |     | 26 | 700  | 11.0 | 2.7 |
|    |      |      |     | 26 | 1300 | 12.0 | 2.8 |
|    |      |      |     | 26 | 1900 | 11.0 | 2.3 |
|    |      |      |     | 27 | 100  | 12.0 | 2.2 |
|    |      |      |     | 27 | 700  | 14.0 | 2.2 |
|    |      |      |     | 27 | 1300 | 12.0 | 2.0 |
|    |      |      |     | 28 | 100  | 12.0 | 1.2 |
|    |      |      |     |    |      |      |     |

|     |      | MARCH 1983 |            |     |      | APRIL 1983 |            |
|-----|------|------------|------------|-----|------|------------|------------|
| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
| 1   | 100  | 8.0        | 1.8        | 1   | 100  | 7.0        | 2.6        |
| 1   | 700  | 11.0       | 2.8        | 1   | 700  | 11.0       | 2.2        |
| 1   | 1300 | 12.0       | 2.1        | 1   | 1300 | 11.0       | 2.0        |
| 1   | 1900 | 10.0       | 2.1        | 1   | 1900 | 10.0       | 2.0        |
| 2   | 100  | 11.0       | 1.5        | 2   | 100  | 12.0       | 1.8        |
| 3   | 100  | 11.0       | 0.9        | 3   | 100  | 8.0        | 1.8        |
| 4   | 100  | 10.0       | 0.6        | 4   | 100  | 11.0       | 0.9        |
| 5   | 100  | 12.0       | 0.4        | 5   | 100  | 9.0        | 0.5        |
| 6   | 100  | 10.0       | 0.6        | 6   | 100  | 9.0        | 0.4        |
| 7   | 100  | 7.0        | 1.0        | 7   | 100  | 14.0       | 0.3        |
| 8   | 100  | 8.0        | 0.6        | 8   | 100  | 9.0        | 0.3        |
| 9   | 100  | 9.0        | 1.2        | 9   | 100  | 8.0        | 0.6        |
| 10  | 100  | 10.0       | 1.2        | 10  | 100  | 11.0       | 1.3        |
| 11  | 100  | 9.0        | 1.0        | 11  | 100  | 13.0       | 1.1        |
| 12  | 100  | 10.0       | 1.6        | 12  | 100  | 10.0       | 0.7        |
| 12  | 1300 | 11.0       | 2.0        | 13  | 100  | 10.0       | 0.6        |
| 13  | 700  | 8.0        | 1.0        | 14  | 100  | 10.0       | 0.7        |
| 14  | 100  | 6.0        | 0.6        | 15  | 100  | 9.0        | 1.0        |
| 15  | 100  | 14.0       | 0.5        | 16  | 100  | 7.0        | 1.2        |
| 16  | 100  | 10.0       | 0.4        | 17  | 100  | 12.0       | 1.3        |
| 17  | 100  | 5.0        | 1.6        | 18  | 100  | 11.0       | 0.9        |
| 17  | 1300 | 8.0        | 2.0        | 19  | 100  | 6.0        | 1.7        |
| 17  | 1900 | 7.0        | 2.4        | 20  | 100  | 10.0       | 0.5        |
| 18  | 100  | 10.0       | 2.8        | 21  | 100  | 4.0        | 0.4        |
| 18  | 700  | 10.0       | 3.3        | 22  | 100  | 9.0        | 0.4        |
| 18  | 1300 | 11.0       | 3.0        | 23  | 100  | 10.0       | 0.5        |
| 18  | 1900 | 11.0       | 2.7        | 24  | 100  | 8.0        | 2.3        |
| 19  | 100  | 11.0       | 2.7        | 25  | 100  | 12.0       | 1.2        |
| 19  | 700  | 11.0       | 2.0        | 26  | 100  | 9.0        | 0.6        |
| 20  | 100  | 11.0       | 1.2        | 27  | 100  | 11.0       | 0.5        |
| 21  | 100  | 12.0       | 0.9        | 28  | 100  | 10.0       | 0.4        |
| 22  | 100  | 10.0       | 0.8        | 29  | 100  | 14.0       | 0.5        |
| 23  | 100  | 4.0        | 0.6        | 30  | 100  | 12.0       | 0.4        |
| 24  | 100  | 11.0       | 0.4        |     |      |            |            |

| 24 | 1900 | 6.0  | 2.2 |
|----|------|------|-----|
| 25 | 100  | 8.0  | 3.2 |
| 25 | 700  | 11.0 | 3.3 |
| 25 | 1300 | 12.0 | 3.3 |
| 25 | 1900 | 14.0 | 3.1 |
| 26 | 100  | 14.0 | 2.8 |
| 26 | 700  | 15.0 | 2.9 |
| 26 | 1300 | 13.0 | 2.8 |
| 26 | 1900 | 13.0 | 2.3 |
| 27 | 100  | 13.0 | 2.4 |
| 27 | 1900 | 12.0 | 2.1 |
| 28 | 100  | 11.0 | 1.9 |
| 29 | 100  | 10.0 | 0.8 |
| 30 | 100  | 5.0  | 0.5 |
| 31 | 100  | 7.0  | 0.8 |
| 31 | 1900 | 6.0  | 2.4 |
|    |      |      |     |

# MAY 1983

#### JUNE 1983

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 100  | 11.0       | 0.5        | 1   | 100  | 9.0        | 0.6        |
| 2   | 100  | 8.0        | 0.6        | 2   | 100  | 5.0        | 0.7        |
| 3   | 100  | 9.0        | 0.8        | 3   | 100  | 10.0       | 0.5        |
| 4   | 100  | 9.0        | 0.7        | 4   | 100  | 14.0       | 0.5        |
| 5   | 100  | 8.0        | 0.5        | 5   | 100  | 12.0       | 0.4        |
| 6   | 100  | 9.0        | 0.4        | 6   | 100  | 9.0        | 0.4        |
| 7   | 100  | 8.0        | 0.6        | 7   | 100  | 6.0        | 0.4        |
| 8   | 100  | 8.0        | 0.5        | 8   | 100  | 7.0        | 0.4        |
| 9   | 700  | 6.0        | 1.3        | 9   | 100  | 6.0        | 0.6        |
| 10  | 100  | 6.0        | 0.6        | 9   | 1900 | 7.0        | 2.0        |
| 11  | 100  | 9.0        | 0.6        | 10  | 100  | 7.0        | 1.8        |
| 12  | 100  | 10.0       | 0.8        | 11  | 100  | 8.0        | 1.1        |
| 13  | 100  | 5.0        | 0.9        | 12  | 100  | 9.0        | 0.9        |
| 14  | 100  | 8.0        | 0.5        | 13  | 100  | 9.0        | 0.6        |
| 15  | 100  | 10.0       | 0.5        | 14  | 100  | 8.0        | 0.4        |
| 16  | 100  | 12.0       | 0.4        | 15  | 100  | 9.0        | 0.5        |
| 17  | 100  | 7.0        | 1.8        | 16  | 100  | 6.0        | 0.5        |
| 18  | 100  | 9.0        | 1.0        | 17  | 100  | 9.0        | 0.6        |
| 19  | 100  | 9.0        | 1.0        | 18  | 100  | 8.0        | 0.8        |
| 20  | 100  | 8.0        | 0.9        | 19  | 100  | 9.0        | 0.9        |
| 21  | 100  | 8.0        | 0.8        | 20  | 100  | 9.0        | 0.8        |
| 22  | 100  | 9.0        | 0.6        | 21  | 100  | 9.0        | 0.6        |
| 23  | 100  | 9.0        | 0.5        | 22  | 100  | 4.0        | 0.9        |
| 24  | 100  | 7.0        | 0.5        | 23  | 100  | 6.0        | 1.1        |
| 25  | 100  | 8.0        | 0.5        | 24  | 100  | 9.0        | 0.8        |
| 26  | 100  | 17.0       | 0.6        | 25  | 100  | 9.0        | 0.5        |
| 27  | 100  | 8.0        | 0.6        | 26  | 100  | 11.0       | 0.3        |
| 28  | 100  | 14.0       | 0.6        | 27  | 100  | 11.0       | 0.3        |
| 29  | 100  | 11.0       | 0.8        | 28  | 100  | 11.0       | 0.3        |
|     |      |            |            |     |      |            |            |

(Continued)

(Sheet 14 of 22)

| 30       | 100        | 10.0          | 0.8        | 29       | 100        | 4.0          | 0.4        |
|----------|------------|---------------|------------|----------|------------|--------------|------------|
| 31       | 100        | 9.0           | 0.7        | 30       | 100        | 7.0          | 1.4        |
|          |            |               |            |          |            |              |            |
|          |            |               |            |          |            |              |            |
|          |            | JULY 1983     |            |          |            | AUGUST 1983  |            |
|          |            |               |            |          |            |              |            |
| DAY      | TIME       | PERIOD (S)    | HEIGHT (M) | DAY      | TIME       | PERIOD (S)   | HEIGHT (M) |
| 1        | 100        | 6.0           | 0.8        | 1        | 100        | 12.0         | 0.3        |
| 2        | 100        | 7.0           | 0.6        | 2        | 100        | 7.0          | 0.4        |
| 3        | 100        | 9.0           | 0.5        | 3        | 100        | 8.0          | 0.4        |
| 4        | 100        | 10.0          | 0.6        | 4        | 100        | 17.0         | 0.3        |
| 5        | 100        | 8.0           | 0.5        | 5        | 100        | 10.0         | 0.9        |
| 6        | 100        | 17.0          | 0.3        | 6        | 100        | 9.0          | 0.6        |
| 7        | 100        | 3.0           | 0.6        | 7        | 100        | 7.0          | 0.6        |
| 8        | 100        | 8.0           | 0.7        | 8        | 100        | 10.0         | 0.4        |
| 9        | 100        | 7.0           | 0.6        | 9        | 100        | 14.0         | 0.4        |
| 10       | 100        | 8.0           | 0.5        | 10       | 100        | 14.0         | 0.3        |
| 11<br>12 | 100        | 6.0           | 0.6        | 11       | 100        | 14.0         | 0.5        |
| 13       | 100<br>100 | 7.0<br>10.0   | 0.4        | 12<br>13 | 100        | 7.0<br>5.0   | 0.4        |
| 14       | 100        | 12.0          | 0.4        | 14       | 100<br>100 | 7.0          | 1.0        |
| 15       | 100        | 10.0          | 0.3        | 15       | 100        | 8.0          | 1.5        |
| 16       | 100        | 10.0          | 0.3        | 16       | 100        | 9.0          | 0.7        |
| 17       | 100        | 10.0          | 0.2        | 17       | 100        | 8.0          | 0.8        |
| 18       | 100        | 10.0          | 0.4        | 18       | 100        | 8.0          | 0.5        |
| 19       | 100        | 10.0          | 0.3        | 19       | 100        | 9.0          | 0.4        |
| 20       | 100        | 10.0          | 0.3        | 20       | 100        | 10.0         | 0.4        |
| 21       | 100        | 10.0          | 0.3        | 21       | 100        | 10.0         | 0.3        |
| 22       | 100        | 7.0           | 0.5        | 22       | 100        | 5.0          | 0.5        |
| 23       | 100        | 8.0           | 0.7        | 23       | 100        | 6.0          | 0.3        |
| 24       | 100        | 8.0           | 0.5        | 24       | 100        | 4.0          | 0.6        |
| 25       | 100        | 10.0          | 0.4        | 25       | 100        | 7.0          | 1.1        |
| 26       | 700        | 14.0          | 0.7        | 26       | 100        | 7.0          | 0.2        |
| 27       | 100        | 14.0          | 0.6        | 27       | 100        | 7.0          | 0.7        |
| 28       | 100        | 14.0          | 0.6        | 28       | 100        | 9.0          | 0.6        |
| 29       | 100        | 8.0           | 0.6        | 29       | 100        | 8.0          | 0.5        |
| 30       | 100        | 7.0           | 0.7        | 30       | 100        | 7.0          | 0.5        |
| 31       | 100        | 10.0          | 0.4        | 31       | 100        | 6.0          | 0.7        |
|          |            |               |            |          |            |              |            |
|          |            |               |            |          |            |              |            |
|          | 5          | SEPTEMBER 198 | 3          |          |            | OCTOBER 1983 |            |
| DAY      | TIME       | PERIOD (S)    | HEIGHT (M) | DAY      | TIME       | PERIOD (S)   | HEIGHT (M) |
| 1        | 100        | 4.0           | 0.9        | 1        | 100        | 11.0         | 0.9        |
| 2        | 100        | 8.0           | 0.7        | 2        | 100        | 10.0         | 0.6        |
| 3        | 100        | 5.0           | 1.1        | 3        | 100        | 10:0         | 0.5        |
| 4        | 100        | 12.0          | 0.5        | 4        | 100        | 14.0         | 0.6        |
| 5        | 100        | 10.0          | 0.6        | 5        | 100        | 14.0         | 0.5        |
| 6        | 100        | 14.0          | 0.4        | 6        | 100        | 14.0         | 0.5        |
|          |            |               |            |          |            |              |            |

| 7  | 100  | 14.0 | 0.4 | 7  | 100  | 14.0 | 0.5 |
|----|------|------|-----|----|------|------|-----|
| 8  | 100  | 11.0 | 0.3 | 8  | 100  | 12.0 | 0.9 |
| 9  | 100  | 6.0  | 0.7 | 9  | 100  | 6.0  | 0.7 |
| 10 | 100  | 10.0 | 0.4 | 10 | 100  | 6.0  | 1.1 |
| 11 | 100  | 8.0  | 0.3 | 10 | 1900 | 7.0  | 2.0 |
| 12 | 100  | 14.0 | 0.2 | 11 | 100  | 9.0  | 2.0 |
| 13 | 100  | 14.0 | 0.3 | 11 | 700  | 9.0  | 2.1 |
| 14 | 100  | 4.0  | 0.5 | 11 | 1300 | 10.0 | 2.0 |
| 15 | 100  | 8.0  | 2.6 | 12 | 100  | 10.0 | 1.9 |
| 15 | 700  | 8.0  | 2.2 | 12 | 700  | 11.0 | 2.0 |
| 15 | 1300 | 7.0  | 2.2 | 13 | 100  | 11.0 | 1.2 |
| 15 | 1900 | 9.0  | 2.0 | 14 | 100  | 11.0 | 1.1 |
| 16 | 100  | 11.0 | 1.7 | 15 | 100  | 11.0 | 0.7 |
| 17 | 100  | 7.0  | 1.1 | 16 | 100  | 9.0  | 0.6 |
| 18 | 100  | 10.0 | 0.7 | 17 | 100  | 11.0 | 0.8 |
| 19 | 100  | 11.0 | 0.6 | 18 | 100  | 10.0 | 0.6 |
| 20 | 100  | 10.0 | 0.4 | 19 | 100  | 9.0  | 0.5 |
| 21 | 100  | 9.0  | 0.5 | 20 | 100  | 5.0  | 1.2 |
| 22 | 100  | 4.0  | 0.9 | 20 | 1300 | 6.0  | 2.0 |
| 23 | 100  | 6.0  | 0.8 | 20 | 1900 | 8.0  | 2.2 |
| 24 | 100  | 10.0 | 0.5 | 21 | 100  | 9.0  | 2.1 |
| 25 | 100  | 4.0  | 0.6 | 21 | 700  | 7.0  | 2.5 |
| 26 | 100  | 8.0  | 0.8 | 21 | 1300 | 10.0 | 2.5 |
| 27 | 100  | 9.0  | 1.5 | 21 | 1900 | 8.0  | 2.3 |
| 28 | 100  | 10.0 | 1.1 | 22 | 100  | 8.0  | 2.1 |
| 28 | 700  | 10.0 | 2.1 | 22 | 700  | 10.0 | 2.1 |
| 28 | 1900 | 9.0  | 2.4 | 23 | 100  | 12.0 | 1.6 |
| 29 | 100  | 11.0 | 2.6 | 24 | 100  | 12.0 | 1.4 |
| 29 | 700  | 11.0 | 2.5 | 25 | 100  | 14.0 | 1.1 |
| 29 | 1300 | 11.0 | 3.0 | 25 | 1300 | 6.0  | 2.0 |
| 29 | 1900 | 12.0 | 2.8 | 25 | 1900 | 7.0  | 2.1 |
| 30 | 100  | 9.0  | 2.5 | 26 | 100  | 10.0 | 1.8 |
|    |      |      |     | 27 | 100  | 12.0 | 1.2 |
|    |      |      |     | 28 | 100  | 6.0  | 0.9 |
|    |      |      |     | 29 | 100  | 11.0 | 0.2 |
|    |      |      |     | 30 | 100  | 6.0  | 1.5 |
|    |      |      |     | 31 | 100  | 7.0  | 0.9 |
|    |      |      |     |    |      |      |     |

#### NOVEMBER 1983

### DECEMBER 1983

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 100  | 8.0        | 0.7        | 1   | 100  | 7.0        | 0.3        |
| 2   | 100  | 7.0        | 0.9        | 2   | 100  | 14.0       | 0.5        |
| 3   | 100  | 7.0        | 0.9        | 3   | 100  | 3.0        | 0.4        |
| 4   | 100  | 11.0       | 0.9        | 4   | 100  | 6.0        | 1.4        |
| 5   | 100  | 12.0       | 1.1        | 5   | 100  | 8.0        | 0.5        |
| 6   | 100  | 14.0       | 0.9        | 6   | 100  | 8.0        | 0.9        |
| 7   | 100  | 12.0       | 0.6        | 7   | 100  | 12.0       | 0.7        |

| 8  | 100 | 12.0 | 0.5 | 8  | 100  | 5.0  | 0.5 |
|----|-----|------|-----|----|------|------|-----|
| 9  | 100 | 14.0 | 0.6 | 9  | 100  | 14.0 | 0.4 |
| 10 | 100 | 9.0  | 1.2 | 10 | 100  | 12.0 | 0.3 |
| 11 | 100 | 9.0  | 0.9 | 11 | 100  | 11.0 | 0.5 |
| 12 | 100 | 9.0  | 0.4 | 12 | 100  | 7.0  | 1.8 |
| 13 | 100 | 6.0  | 1.0 | 12 | 700  | 11.0 | 2.1 |
| 14 | 100 | 6.0  | 0.6 | 12 | 1300 | 9.0  | 2.9 |
| 15 | 100 | 5.0  | 0.4 | 12 | 1900 | 10.0 | 2.3 |
| 16 | 100 | 11.0 | 1.1 | 13 | 100  | 11.0 | 2.0 |
| 17 | 100 | 9.0  | 0.3 | 13 | 700  | 9.0  | 2.0 |
| 18 | 100 | 4.0  | 0.5 | 14 | 700  | 11.0 | 1.0 |
| 19 | 100 | 12.0 | 0.3 | 15 | 100  | 9.0  | 0.7 |
| 20 | 100 | 11.0 | 0.2 | 16 | 700  | 10.0 | 0.5 |
| 21 | 100 | 8.0  | 0.8 | 17 | 100  | 10.0 | 0.5 |
| 22 | 100 | 9.0  | 0.5 | 18 | 100  | 17.0 | 0.9 |
| 23 | 100 | 12.0 | 0.3 | 19 | 100  | 6.0  | 1.7 |
| 24 | 100 | 12.0 | 0.3 | 19 | 700  | 6.0  | 2.0 |
| 25 | 100 | 7.0  | 0.7 | 19 | 1300 | 7.0  | 2.6 |
| 26 | 100 | 10.0 | 0.4 | 20 | 100  | 9.0  | 2.0 |
| 27 | 100 | 10.0 | 0.2 | 21 | 100  | 7.0  | 1.7 |
| 28 | 100 | 12.0 | 0.3 | 21 | 1300 | 6.0  | 2.2 |
| 29 | 100 | 5.0  | 0.6 | 22 | 100  | 7.0  | 1.8 |
| 30 | 100 | 7.0  | 0.3 | 22 | 1300 | 10.0 | 2.1 |
|    |     |      |     | 23 | 100  | 10.0 | 1.0 |
|    |     |      |     | 24 | 100  | 5.0  | 1.2 |
|    |     |      |     | 25 | 100  | 7.0  | 1.6 |
|    |     |      |     | 26 | 100  | 5.0  | 0.8 |
|    |     |      |     | 27 | 100  | 9.0  | 0.3 |
|    |     |      |     | 28 | 100  | 14.0 | 0.1 |
|    |     |      |     | 29 | 100  | 9.0  | 0.5 |
|    |     |      |     | 30 | 100  | 8.0  | 1.4 |
|    |     |      |     | 31 | 100  | 7.0  | 1.7 |
|    |     |      |     |    |      |      |     |

| JANUARY 1984 | FEBRUARY 198 |
|--------------|--------------|
|              |              |

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 100  | 10.0       | 2.1        | 1   | 100  | 6.0        | 0.9        |
| 1   | 700  | 11.0       | 2.0        | 2   | 100  | 11.0       | 0.6        |
| 1   | 1300 | 11.0       | 2.3        | 3   | 100  | 11.0       | 0.5        |
| 2   | 100  | 7.0        | 1.9        | 4   | 100  | 7.0        | 1.0        |
| 3   | 100  | 11.0       | 1.2        | 5   | 100  | 8.0        | 0.8        |
| 4   | 100  | 12.0       | 1.1        | 6   | 100  | 9.0        | 0.6        |
| 5   | 100  | 11.0       | 0.7        | 7   | 100  | 6.0        | 1.1        |
| 6   | 100  | 5.0        | 0.5        | 8   | 100  | 6.0        | 1.0        |
| 7   | 100  | 9.0        | 0.4        | 9   | 100  | 8.0        | 0.6        |
| 8   | 100  | 5.0        | 0.9        | 10  | 100  | 10.0       | 0.3        |
| 9   | 100  | 10.0       | 0.3        | 11  | 100  | 10.0       | 0.4        |

| 10 | 100  | 5.0  | 0.6 | 12 | 100  | 11.0 | 0.5 |
|----|------|------|-----|----|------|------|-----|
| 11 | 100  | 8.0  | 1.5 | 13 | 100  | 6.0  | 0.4 |
| 11 | 700  | 7.0  | 2.3 | 14 | 100  | 8.0  | 1.4 |
| 11 | 1300 | 9.0  | 2.5 | 14 | 1300 | 10.0 | 2.0 |
| 11 | 1900 | 10.0 | 2.7 | 14 | 1900 | 11.0 | 2.0 |
| 12 | 100  | 7.0  | 2.6 | 15 | 100  | 10.0 | 2.5 |
| 12 | 700  | 9.0  | 2.7 | 16 | 100  | 10.0 | 1.4 |
| 12 | 1300 | 9.0  | 2.4 | 17 | 100  | 9.0  | 0.8 |
| 12 | 1900 | 6.0  | 2.6 | 18 | 100  | 10.0 | 0.9 |
| 13 | 100  | 11.0 | 2.1 | 19 | 100  | 10.0 | 0.7 |
| 13 | 700  | 9.0  | 2.1 | 20 | 100  | 8.0  | 0.5 |
| 13 | 1900 | 12.0 | 2.1 | 21 | 100  | 10.0 | 0.5 |
| 14 | 100  | 12.0 | 2.1 | 22 | 100  | 11.0 | 0.7 |
| 14 | 700  | 11.0 | 2.0 | 23 | 700  | 3.0  | 0.8 |
| 15 | 100  | 12.0 | 2.0 | 23 | 1300 | 7.0  | 2.0 |
| 16 | 100  | 10.0 | 1.4 | 24 | 100  | 11.0 | 0.9 |
| 17 | 100  | 11.0 | 0.9 | 25 | 100  | 11.0 | 0.4 |
| 18 | 100  | 9.0  | 0.8 | 26 | 100  | 7.0  | 0.5 |
| 19 | 100  | 9.0  | 1.5 | 27 | 100  | 5.0  | 0.6 |
| 20 | 100  | 7.0  | 1.1 | 28 | 100  | 9.0  | 2.3 |
| 21 | 100  | 10.0 | 0.7 | 29 | 100  | 10.0 | 0.6 |
| 22 | 100  | 6.0  | 1.1 |    |      |      |     |
| 23 | 100  | 4.0  | 0.8 |    |      |      |     |
| 24 | 100  | 10.0 | 0.7 |    |      |      |     |
| 25 | 100  | 9.0  | 1.1 |    |      |      |     |
| 26 | 100  | 11.0 | 0.6 |    |      |      |     |
| 27 | 100  | 11.0 | 0.6 |    |      |      |     |
| 28 | 100  | 10.0 | 0.8 |    |      |      |     |
| 29 | 100  | 6.0  | 1.2 |    |      |      |     |
| 30 | 100  | 9.0  | 0.6 |    |      |      |     |
| 31 | 100  | 9.0  | 0.4 |    |      |      |     |
|    |      |      |     |    |      |      |     |

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M) |
|-----|------|------------|------------|-----|------|------------|------------|
| 1   | 100  | 4.0        | 0.7        | 1   | 100  | 11.0       | 1.2        |
| 2   | 100  | 12.0       | 0.3        | 2   | 100  | 12.0       | 0.8        |
| 3   | 100  | 10.0       | 0.2        | 3   | 100  | 11.0       | 0.6        |
| 4   | 100  | 6.0        | 0.6        | 4   | 100  | 10.0       | 0.9        |
| 5   | 100  | 14.0       | 0.7        | 5   | 100  | 11.0       | 1.5        |
| 6   | 100  | 7.0        | 0.7        | 5   | 1300 | 12.0       | 2.0        |
| 7   | 100  | 6.0        | 1.4        | 6   | 100  | 12.0       | 1.0        |
| 8   | 100  | 12.0       | 0.8        | 7   | 100  | 9.0        | 0.7        |
| 9   | 100  | 7.0        | 0.5        | 8   | 100  | 11.0       | 0.7        |
| 10  | 100  | 10.0       | 1.2        | 9   | 100  | 11.0       | 0.7        |
| 12  | 1300 | 6.0        | 1.4        | 10  | 100  | 6.0        | 1.4        |
| 13  | 700  | 7.0        | 1.4        | 11  | 100  | 9.0        | 1.1        |
| 13  | 1900 | 10.0       | 2.0        | 12  | 100  | 7.0        | 1.0        |

MARCH 1984

(Continued)

APRIL 1984

| 14 | 100 | 10.0 | 1.6 | 13 | 100 | 11.0 | 0.8 |
|----|-----|------|-----|----|-----|------|-----|
| 15 | 100 | 10.0 | 0.8 | 14 | 100 | 9.0  | 0.8 |
| 16 | 100 | 12.0 | 0.8 | 15 | 100 | 8.0  | 0.8 |
| 17 | 100 | 12.0 | 1.1 | 16 | 100 | 12.0 | 1.2 |
| 18 | 100 | 7.0  | 1.8 | 17 | 100 | 9.0  | 0.8 |
| 19 | 100 | 12.0 | 1.5 | 18 | 100 | 11.0 | 0.5 |
| 20 | 100 | 14.0 | 1.1 | 19 | 100 | 11.0 | 0.5 |
| 21 | 100 | 10.0 | 1.0 | 20 | 100 | 9.0  | 0.4 |
| 22 | 100 | 11.0 | 0.7 | 21 | 100 | 10.0 | 0.4 |
| 23 | 100 | 11.0 | 0.5 | 22 | 100 | 10.0 | 0.3 |
| 24 | 100 | 11.0 | 0.3 | 23 | 100 | 11.0 | 1.2 |
| 25 | 100 | 6.0  | 0.5 | 24 | 100 | 12.0 | 1.0 |
| 26 | 100 | 7.0  | 0.6 | 25 | 100 | 11.0 | 0.5 |
| 27 | 100 | 10.0 | 1.4 | 26 | 100 | 12.0 | 0.3 |
| 28 | 100 | 9.0  | 0.8 | 27 | 100 | 11.0 | 0.4 |
| 29 | 100 | 10.0 | 1.2 | 28 | 100 | 10.0 | 1.0 |
| 30 | 100 | 8.0  | 1.4 | 29 | 100 | 11.0 | 1.3 |
| 31 | 100 | 12.0 | 1.1 | 30 | 100 | 11.0 | 1.2 |
|    |     |      |     |    |     |      |     |

| MAY 1984 | JUNE 1984 |
|----------|-----------|
|          |           |

| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S) | HEIGHT (M)  |
|-----|------|------------|------------|-----|------|------------|-------------|
| 1   | 700  | 11.0       | 0.7        | 1   | 100  | 10.0       | 1.0         |
| 2   | 700  | 10.0       | 0.5        | 2   | 100  | 6.0        | 0.7         |
| 3   | 100  | 9.0        | 0.4        | 3   | 100  | 7.0        | 0.6         |
| 4   | 100  | 7.0        | 0.8        | 4   | 100  | 11.0       | 0.5         |
| 5   | 100  | 11.0       | 0.8        | 5   | 100  | 11.0       | 0.6         |
| 6   | 100  | 8.0        | 0.4        | 6   | 100  | 10.0       | 0.5         |
| 7   | 100  | 7.0        | 0.4        | 7   | 100  | 10.0       | 0.4         |
| 8   | 100  | 7.0        | 0.5        | 8   | 100  | 10.0       | 0.3         |
| 9   | 100  | 4.0        | 0.7        | 9   | 700  | 9.0        | 0.3         |
| 10  | 100  | 7.0        | 0.4        | 10  | 100  | 9.0        | 0.3         |
| 11  | 100  | 6.0        | 0.4        | 11  | 100  | 7.0        | 0.3         |
| 12  | 100  | 8.0        | 0.3        | 12  | 100  | 8.0        | 0.3         |
| 13  | 100  | 9.0        | 0.4        | 13  | 100  | 10.0       | 0.4         |
| 14  | 100  | 8.0        | 0.4        | 14  | 100  | 10.0       | 0.3         |
| 15  | 100  | 6.0        | 1.5        | 15  | 100  | 9.0        | 0.3         |
| 16  | 100  | 3.0        | 0.7        | 16  | 100  | 6.0        | 0.6         |
| 17  | 100  | 6.0        | 0.6        | 17  | 100  | 5.0        | 0.8         |
| 18  | 100  | 8.0        | 1.1        | 18  | 100  | 7.0        | 0.4         |
| 19  | 100  | 12.0       | 1.9        | 19  | 100  | 9.0        | 0.4         |
| 20  | 1300 | 11.0       | 0.4        | 20  | 100  | 9.0        | 0.6         |
| 21  | 100  | 9.0        | 0.3        | 21  | 100  | 9.0        | <b>0.</b> 6 |
| 22  | 100  | 10.0       | 0.3        | 22  | 100  | 7.0        | 0.7         |
| 23  | 700  | 10.0       | 0.4        | 23  | 100  | 5.0        | 0.9         |

| 24 | 100 | 5.0 | 0.7 | 24 | 100 | 4.0  | 0.8 |
|----|-----|-----|-----|----|-----|------|-----|
| 25 | 100 | 7.0 | 0.6 | 25 | 100 | 7.0  | 0.9 |
| 26 | 100 | 6.0 | 0.6 | 26 | 100 | 10.0 | 8.0 |
| 27 | 100 | 7.0 | 0.6 | 27 | 100 | 9.0  | 0.7 |
| 28 | 100 | 9.0 | 0.5 | 28 | 100 | 9.0  | 0.7 |
| 29 | 100 | 6.0 | 0.7 | 29 | 100 | 11.0 | 0.5 |
| 30 | 100 | 8.0 | 1.0 | 30 | 100 | 7.0  | 0.6 |
| 31 | 100 | 6.0 | 1.8 |    |     |      |     |
| 31 | 700 | 6.0 | 2.1 |    |     |      |     |

|     |      | JULY 1984  |            |     |      | AUGUST 1984 |            |
|-----|------|------------|------------|-----|------|-------------|------------|
| DAY | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME | PERIOD (S)  | HEIGHT (M) |
| 1   | 100  | 9.0        | 0.6        | 1   | 100  | 8.0         | 0.5        |
| 2   | 100  | 8.0        | 0.5        | 2   | 100  | 10.0        | 0.5        |
| 3   | 100  | 9.0        | 0.5        | 3   | 100  | 10.0        | 0.3        |
| 4   | 100  | 8.0        | 0.4        | 4   | 100  | 8.0         | 0.3        |
| 5   | 100  | 9.0        | 0.5        | 5   | 100  | 14.0        | 0.3        |
| 6   | 100  | 6.0        | 0.6        | 6   | 100  | 9.0         | 0.3        |
| 7   | 100  | 7.0        | 0.9        | 7   | 100  | 9.0         | 0.3        |
| 8   | 100  | 8.0        | 0.7        | 8   | 100  | 9.0         | 0.3        |
| 9   | 100  | 8.0        | 0.8        | 9   | 100  | 9.0         | 0.3        |
| 10  | 100  | 7.0        | 0.6        | 10  | 100  | 7.0         | 0.3        |
| 11  | 100  | 10.0       | 0.4        | 11  | 100  | 5.0         | 0.4        |
| 12  | 100  | 9.0        | 0.4        | 12  | 100  | 8.0         | 0.4        |
| 13  | 100  | 9.0        | 0.3        | 13  | 100  | 8.0         | 0.5        |
| 14  | 100  | 12.0       | 0.3        | 14  | 1300 | 5.0         | 0.5        |
| 15  | 100  | 7.0        | 0.3        | 15  | 100  | 7.0         | 0.4        |
| 16  | 100  | 9.0        | 0.4        | 16  | 100  | 7.0         | 0.5        |
| 17  | 100  | 10.0       | 0.4        | 17  | 100  | 8.0         | 0.4        |
| 18  | 100  | 9.0        | 0.5        | 18  | 100  | 10.0        | 0.4        |
| 19  | 100  | 8.0        | 0.5        | 19  | 100  | 9.0         | 0.5        |
| 20  | 100  | 17.0       | 0.5        | 20  | 100  | 10.0        | 0.3        |
| 21  | 100  | 17.0       | 0.5        | 21  | 100  | 6.0         | 1.0        |
| 22  | 100  | 14.0       | 0.6        | 22  | 100  | 6.0         | 0.6        |
| 23  | 100  | 7.0        | 0.7        | 23  | 100  | 5.0         | 0.6        |
| 24  | 100  | 12.0       | 0.5        | 24  | 100  | 6.0         | 0.4        |
| 25  | 100  | 14.0       | 0.3        | 25  | 100  | 6.0         | 0.6        |
| 26  | 100  | 14.0       | 0.3        | 26  | 100  | 6.0         | 1.3        |
| 27  | 100  | 14.0       | 0.4        | 27  | 100  | 8.0         | 1.0        |
| 28  | 100  | 9.0        | 0.4        | 28  | 100  | 10.0        | 0.6        |
| 29  | 100  | 4.0        | 0.8        | 29  | 700  | 8.0         | 0.5        |
| 30  | 100  | 5.0        | 0.8        | 30  | 100  | 9.0         | 0.4        |
| 31  | 100  | 6.0        | 0.6        | 31  | 700  | 10.0        | 0.3        |
|     |      |            |            |     |      |             |            |

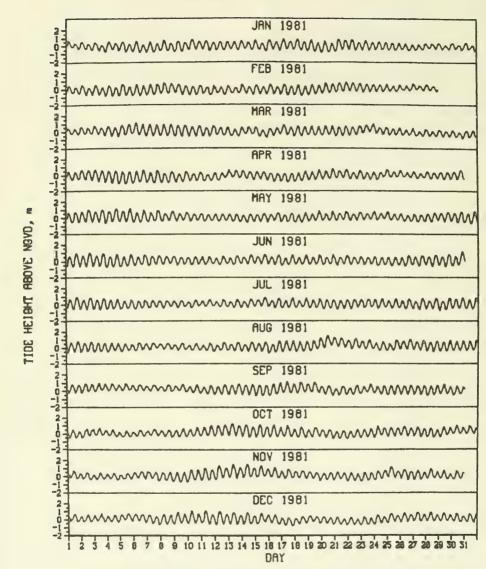
| SEPTEMBER 1984 |            |            |            |          | OCTOBER 1984 |              |            |  |
|----------------|------------|------------|------------|----------|--------------|--------------|------------|--|
| DAY            | TIME       | PERIOD (S) | HEIGHT (M) | DAY      | TIME         | PERIOD (S)   | HEIGHT (M) |  |
| 1              | 100        | 8.0        | 0.3        | 1        | 100          | 10.0         | 1.7        |  |
| 2              | 100        | 17.0       | 0.4        | 2        | 100          | 10.0         | 1.3        |  |
| 3              | 700        | 17.0       | 0.3        | 3        | 100          | 9.0          | 0.9        |  |
| 4              | 100        | 14.0       | 0.4        | 4        | 100          | 11.0         | 0.4        |  |
| 5              | 100        | 5.0        | 0.8        | 5        | 100          | 11.0         | 0.4        |  |
| 6              | 100        | 6.0        | 0.9        | 6        | 100          | 10.0         | 0.5        |  |
| 7              | 100        | 6.0        | 1.2        | 7        | 100          | 6.0          | 1.5        |  |
| 8              | 100        | 9.0        | 1.0        | 8        | 100          | 5.0          | 0.9        |  |
| 9              | 100        | 6.0        | 1.4        | 9        | 100          | 9.0          | 0.7        |  |
| 10             | 100        | 7.0        | 1.2        | 10       | 100          | 10.0         | 0.9        |  |
| 11             | 100        | 8.0        | 1.1        | 11       | 100          | 12.0         | 1.6        |  |
| 12             | 100        | 7.0        | 0.8        | 11       | 1300         | 9.0          | 2.0        |  |
| 13             | 100        | 5.0        | 1.0        | 11       | 1900         | 9.0          | 2.2        |  |
| 14             | 100        | 6.0        | 0.8        | 12       | 100          | 10.0         | 2.3        |  |
| 15             | 100        | 7.0        | 1.3        | 12       | 700          | 9.0          | 2.3        |  |
| 16             | 100        | 6.0        | 1.6        | 12       | 1300         | 11.0         | 2.5        |  |
| 17             | 100        | 7.0        | 1.9        | 12       | 1900         | 12.0         | 2.7        |  |
| 18             | 100        | 8.0        | 1.7        | 13       | 100          | 12.0         | 2.9        |  |
| 19             | 100        | 10.0       | 1.3        | 13       | 700          | 12.0         | 3.2        |  |
| 20             | 700        | 9.0        | 1.0        | 13       | 1300         | 12.0         | 3.3        |  |
| 21             | 100        | 11.0       | 0.8        | 13       | 1900         | 14.0         | 3.3        |  |
| 22             | 100        | 9.0        | 0.7        | 14       | 100          | 14.0         | 3.2        |  |
| 23             | 100        | 9.0        | 0.8        | 14       | 700          | 14.0         | 3.0        |  |
| 24             | 100        | 12.0       | 0.6        | 14       | 1300         | 12.0         | 2.8        |  |
| 25             | 100        | 11.0       | 0.6        | 14       | 1900         | 12.0         | 2.5        |  |
| 26<br>27       | 100<br>100 | 10.0       | 0.5<br>1.9 | 15<br>15 | 100<br>700   | 12.0         | 2.7        |  |
| 27             | 700        | 6.0<br>7.0 | 2.0        | 15       | 1300         | 12.0<br>12.0 | 2.1        |  |
| 28             | 100        | 9.0        | 1.4        | 16       | 100          | 12.0         | 1.6        |  |
| 29             | 100        | 10.0       | 1.3        | 17       | 100          | 12.0         | 1.6        |  |
| 29             | 1900       | 7.0        | 2.5        | 17       | 1900         | 14.0         | 2.0        |  |
| 30             | 100        | 9.0        | 2.7        | 18       | 100          | 17.0         | 1.5        |  |
| 30             | 700        | 10.0       | 2.5        | 18       | 1300         | 14.0         | 2.1        |  |
| 30             | 1300       | 11.0       | 2.5        | 19       | 100          | 17.0         | 1.7        |  |
| 30             | 1900       | 10.0       | 2.2        | 20       | 100          | 14.0         | 1.1        |  |
|                |            |            |            | 21       | 100          | 11.0         | 0.8        |  |
|                |            |            |            | 22       | 100          | 10.0         | 0.4        |  |
|                |            |            |            | 23       | 100          | 11.0         | 0.4        |  |
|                |            |            |            | 24       | 100          | 9.0          | 0.4        |  |
|                |            |            |            | 25       | 100          | 7.0          | 0.5        |  |
|                |            |            |            | 26       | 100          | 11.0         | 0.9        |  |
|                |            |            |            | 27       | 100          | 11.0         | 0.8        |  |
|                |            |            |            | 28       | 100          | 10-,0        | 0.6        |  |
|                |            |            |            | 29       | 100          | 10.0         | 0.5        |  |
|                |            |            |            | 30       | 100          | 10.0         | 0.6        |  |
|                |            |            |            | 31       | 100          | 9.0          | 0.9        |  |

Table El. (Concluded)

| NOVEMBER 1984 |      |            |            |     | DECEMBER 1984 |            |            |  |
|---------------|------|------------|------------|-----|---------------|------------|------------|--|
| DAY           | TIME | PERIOD (S) | HEIGHT (M) | DAY | TIME          | PERIOD (S) | HEIGHT (M) |  |
| 1             | 100  | 4.0        | 1.3        | 1   | 100           | 11.0       | 0.5        |  |
| 2             | 100  | 7.0        | 1.1        | 2   | 100           | 10.0       | 0.3        |  |
| 3             | 100  | 6.0        | 2.2        | 3   | 100           | 5.0        | 0.8        |  |
| 3             | 700  | 7.0        | 2.1        | 4   | 100           | 7.0        | 0.4        |  |
| 3             | 1300 | 7.0        | 2.1        | 5   | 1300          | 6.0        | 1.5        |  |
| 4             | 100  | 8.0        | 1.8        | 6   | 100           | 9.0        | 2.2        |  |
| 5             | 100  | 10.0       | 1.5        | 7   | 100           | 6.0        | 1.0        |  |
| 6             | 700  | 10.0       | 1.0        | 8   | 100           | 5.0        | 0.6        |  |
| 7             | 100  | 6.0        | 1.5        | 9   | 100           | 6.0        | 0.3        |  |
| 8             | 100  | 6.0        | 1.2        | 10  | 100           | 10.0       | 0.3        |  |
| 9             | 100  | 10.0       | 1.4        | 11  | 100           | 9.0        | 0.5        |  |
| 10            | 100  | 10.0       | 0.9        | 12  | 100           | 5.0        | 0.8        |  |
| 11            | 100  | 10.0       | 1.0        | 13  | 100           | 9.0        | 0.5        |  |
| 12            | 1300 | 12.0       | 1.2        | 14  | 100           | 10.9       | 0.7        |  |
| 13            | 100  | 12.0       | 0.9        | 15  | 100           | 12.3       | 1.2        |  |
| 14            | 100  | 14.0       | 1.5        | 16  | 100           | 9.7        | 1.0        |  |
| 15            | 100  | 7.0        | 0.8        | 17  | 100           | 9.8        | 0.9        |  |
| 16            | 100  | 11.0       | 0.4        | 18  | 100           | 10.9       | 0.9        |  |
| 17            | 100  | 5.0        | 1.1        | 19  | 100           | 9.8        | 0.6        |  |
| 18            | 100  | 5.0        | 0.5        | 20  | 100           | 12.3       | 0.9        |  |
| 19            | 100  | 5.0        | 0.4        | 21  | 100           | 12.3       | 0.8        |  |
| 20            | 100  | 6.0        | 1.7        | 22  | 100           | 10.9       | 0.7        |  |
| 20            | 700  | 6.0        | 2.1        | 23  | 100           | 9.8        | 0.4        |  |
| 21            | 100  | 7.0        | 1.8        | 24  | 100           | 4.5        | 0.8        |  |
| 22            | 100  | 4.0        | 1.2        | 25  | 100           | 9.8        | 0.6        |  |
| 23            | 100  | 6.0        | 1.5        | 26  | 100           | 6.9        | 1.6        |  |
| 24            | 100  | 4.0        | 1.2        | 27  | 100           | 8.8        | 0.9        |  |
| 25            | 100  | 6.0        | 0.8        | 28  | 100           | 8.8        | 0.5        |  |
| 26            | 100  | 8.0        | 0.6        | 29  | 100           | 10.9       | 0.4        |  |
| 27            | 100  | 8.0        | 0.6        | 30  | 100           | 9.8        | 0.4        |  |
| 28            | 100  | 9.0        | 0.6        | 31  | 100           | 6.4        | 1.1        |  |
| 29            | 100  | 8.0        | 0.8        |     |               |            |            |  |
| 30            | 100  | 11.0       | 0.7        |     |               |            |            |  |

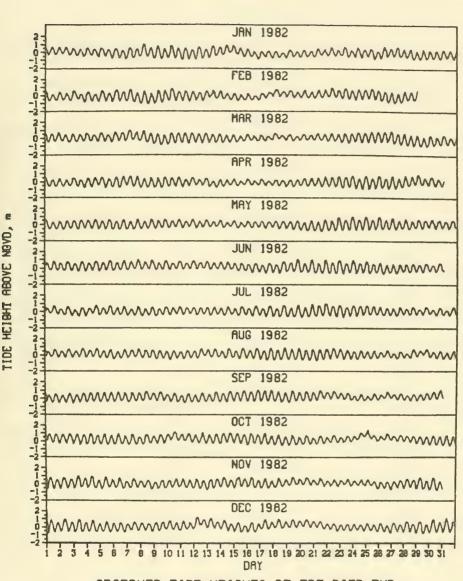
#### APPENDIX F: TIDE LEVELS AT PIER END, 1981-1984

This appendix contains plots of the observed tide levels at the end of the FRF pier. The data are collected by the National Oceanic and Atmospheric Administration/National Ocean Service (NOS) as part of their nationwide tide gaging program. Missing data have been interpolated by NOS. The tide gage, being located near the end of the pier, is occasionally within the surf zone. Thus, the tide data are influenced by setup, setdown, and storm surges, depending on the conditions at the time of the measurement.



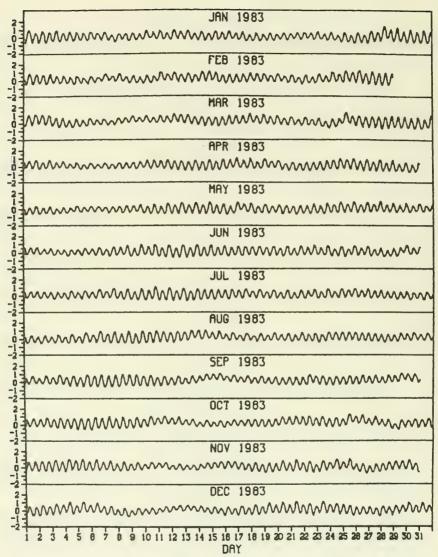
OBSERVED TIDE HEIGHTS AT FRF PIER END

Figure Fl. Tide level record, 1981



OBSERVED TIDE HEIGHTS AT FRF PIER END Figure F2. Tide level record, 1982

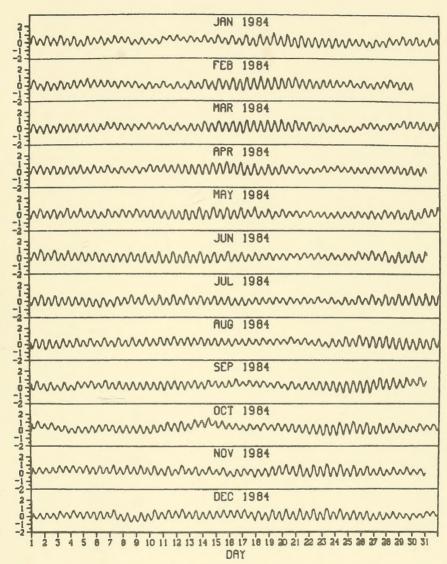




OBSERVED TIDE HEIGHTS AT FRF PIER END

Figure F3. Tide level record, 1983





OBSERVED TIDE HEIGHTS AT FRF PIER END

Figure F4. Tide level record, 1984



